

# **Mass transfer**

#### **Lecture 15:** *Gas absorption*

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## **Learning objectives**

- **Apply the appropriate rate law in analyzing the absorption (or desorption) process, mainly with respect to column height and number of plates.**
- **Predict how temperature, pressure variations can affect the operation in a semi-quantitative manner based on graphs.**

## **Today's outline**

#### • **Gas absorption**

- $\checkmark$  Rate of absorption
- $\checkmark$  Tower height
- $\checkmark$  Number of transfer units
- $\checkmark$  Film coefficients
- $\checkmark$  Effects of pressure
- $\checkmark$  Temperature variations
- $\checkmark$  Multicomponent case
- $\checkmark$  Desorption

### **18.3 Rate of absorption**

• **Volumetric coefficients are often used. For lean gases (y < 0.1), neglecting changes in flow rates results in:** 

 $r = k_y a (y - y_i) = k_x a (x_i - x) = K_y a (y - y^*) = K_x a (x^* - x)$ 

where *a* is the interfacial area per unit volume

 $\checkmark$  The overall coefficients can be obtained using the following relations:

$$
\frac{1}{K_y a} = \frac{1}{k_y a} + \frac{m}{k_x a}, \quad \frac{1}{K_x a} = \frac{1}{k_x a} + \frac{1}{m k_y a}
$$

where *m* is the local slope of the equilibrium curve.

 $\checkmark$  For similar magnitudes of  $k_y a$  and  $k_x a$ , either liquid or gas film can be the source of *controlling resistance*. (e.g., m = 0.1 vs 100)

## **18.3 Tower height**

- **While any of the four eqn.s can be used, the gas-film coefficients are often used.** 
	- For the cross-sectional area of *S*, the amount absorbed in section d*Z* is as follows if the change in flow rates can be neglected:

$$
-V dy = K_y a (y - y^*) S dZ
$$

 $\checkmark$  Integration can be done as follows:  $K_y a S$  $\frac{1}{V} \int_{b}^{c}$  $\int_{0}^{a} dZ =$  $K_{\mathcal{Y}}a S Z_T$  $\frac{\log Z_T}{V} = \int_a^b \frac{dy}{(y-y)^2}$  $y-y^*$ 

$$
\checkmark \quad \text{Lower height, } Z_T, \text{ then becomes}
$$
\n
$$
Z_T = \frac{V}{K_y a s} \int_a^b \frac{dy}{(y - y^*)} \left[ = \right] \frac{mol/s}{\frac{mol}{s} m^2} = m
$$
\n
$$
= H_{0y} N_{0y}
$$

where  $H_{O<sub>V</sub>}$  is the height of transfer unit and  $N_{Ov}$  the number of transfer units.

*Hox & Nox, H<sup>x</sup> & N<sup>x</sup> , H<sup>y</sup> & Ny*?



### **18.3 Number of transfer units**

#### • **When the operating and equilibrium line are straight,**

- $\checkmark$  The number of transfer units (NTU) is the change in conc. across the tower divided by the logarithmic mean driving force.
- $\checkmark$  Unless both lines are also parallel, more units are needed than the number of theoretical plates (NTP).



#### **18.3 Film coefficients**

• In literature,  $k<sub>L</sub>a$  or  $K<sub>q</sub>a$  are often used instead.

 $\checkmark$  The following relations hold between  $k_q$ *a* and  $k_q$ *a*:

$$
K_g a = \frac{K_y a}{P}, \ k_g a = \frac{\breve{k}_y a}{P} \begin{bmatrix} = \end{bmatrix} ?
$$

where *P* is the total pressure.

 $\checkmark$  A similar relationship holds between  $k_i$  a and  $k_x$ a :

$$
K_L a = \frac{K_x a}{\rho}, \ k_L a = \frac{k_x a}{\rho} \left[ = \right]
$$
?

where  $\rho$  is the density of liquid.

• **Mass velocities can also be used in place of** *V* **or** *L*.

$$
\check{G}_M = G_y/M = \frac{u_0 \rho_y}{M} = \frac{\frac{m g}{s m^3}}{\frac{g}{m o l}} = \frac{m o l}{s m^2} = \frac{V}{S}
$$

where *M* is the average molecular weight of the gas

$$
\checkmark H_{Oy} = \frac{V}{K_y a s} = \frac{G_M}{K_g a P}
$$

### **18.3 Effects of pressure**

• **Absorption columns are often operated under high pressure to increase mass transfer rates and capacity.** 

 $\checkmark$   $\checkmark$  varies inversely with the total pressure:

$$
y_A = \frac{p_A}{P}
$$

where *P* is the total pressure.

(1) Why do slopes decrease?

(2) What happens to the overall mass transfer coefficient *Kya*?

(3) Does mass transfer become better or worse?



**FIGURE 18.14** Effect of pressure on absorption.

### **18.3 Temperature variations**

#### • **Two phenomena affects temperature.**

- $\checkmark$  Heat of absorption raises the liquid phase temperature while evaporation tends to lower temperature.
- $\checkmark$  Temperature profile is thus a function of absorption, evaporation and possibly condensation rates across the tower.

#### • **Exact calculation is computationally heavy**.

 $\checkmark$  To simplify, assume the gas inlet T is comparable to liquid outlet T.

(1) Why is the eq. line curved up?

(2) How will this graph change if there is evaporation near the bottom?



• Operation of an absorption column <https://www.youtube.com/watch?v=NhPqSWUrGsg>

#### **18.4 Multicomponent case**

#### • **When more than one solute is absorbed from the gas,**

 $\checkmark$  separate equilibrium and operating lines are needed for each solute.

(1) How are the slopes of the operating lines?

(2) How many transfer units are required for A vs B?

 $\checkmark$  The analysis can be complex especially if the equilibrium of A Is affected by B (or vice versa), or the molar flow rates vary throughout the tower.



### **18.4 Desorption**

#### • **The solutes in the liquid are often desorbed afterwards.**

- $\checkmark$  This produces concentrated solute, as well as regenerated solution for future use.
- $\checkmark$  Desorption can be done by simply (1) lowering ??, (2) raising the ?? or doing both.

 $\checkmark$  The height of a stripping column can be calculated similarly:

$$
Z_T = \frac{L}{K_x a s} \int_a^b \frac{dx}{(x^*-x)} \left[ = \right] \frac{mol/s}{\frac{mol}{s m^3} m^2} = m
$$

$$
= H_{0x} N_{0x}
$$