

# Lecture 7.

## Single Equilibrium Stages (3)

### [Ch. 4]

- Multicomponent Liquid–Liquid Systems
- Solid–Liquid Systems
  - Leaching
  - Crystallization
  - Liquid adsorption
- Gas–Liquid Systems
- Gas–Solid Systems
- Multiphase Systems
  - Vapor–liquid–solid system
  - Vapor–liquid–liquid system

# Multicomponent Liquid–Liquid Systems

- Liquid–liquid extraction process with (1) quaternary and higher component mixtures and/or (2) two solvents
- Equilibria are very complex : no compact graphical way  
 ⇒ computer–assisted algorithm using activity coefficient equations

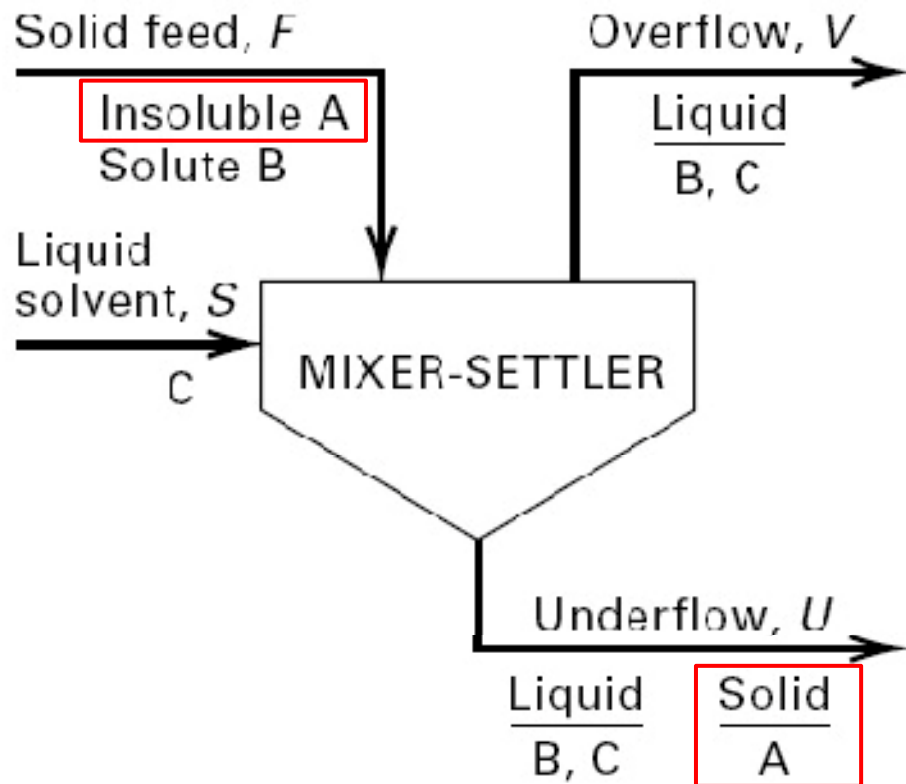
Vapor–Liquid Equilibria	Liquid–Liquid Equilibria
Feed, F	Feed, F + solvent, S
Equilibrium vapor, V	Extract, E (L <sup>(1)</sup> )
Equilibrium liquid, L	Raffinate, R (L <sup>(2)</sup> )
Feed mole fraction, $z_i$	Mole fractions of combined F and S
Vapor mole fractions, $y_i$	Extract mole fractions, $x_i^{(1)}$
Liquid mole fractions, $x_i$	Raffinate mole fractions, $x_i^{(2)}$
K–value, $K_i$	Distribution coefficient, $K_{Di}$
$\Psi = V / F$	$\Psi = E / (F + S)$

# Solid–Liquid Systems

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- **Leaching** (solid–liquid extraction)
  - Separation of multicomponent solid mixture by contacting the solid with a **solvent** that selectively dissolves some components
  - Diffusion in solids is very slow compared to diffusion in liquid
  - Complete separation of a solid phase from a liquid phase is virtually impossible
- **Crystallization**
  - Analogous to distillation
  - Sharp phase separation is virtually impossible
- **Liquid adsorption**
  - The **porous solid agent** selectively adsorbs certain components of the liquid mixture on its exterior and interior surface
- **Membrane–separation**
  - A solid **membrane** absorbs and transports certain species of the liquid mixture

# Leaching



- In an ideal equilibrium leaching stage,
  - Overflow is free of solid
  - None of the solid A is dissolved
  - The composition of the underflow liquid phase is same as the composition of the overflow liquid

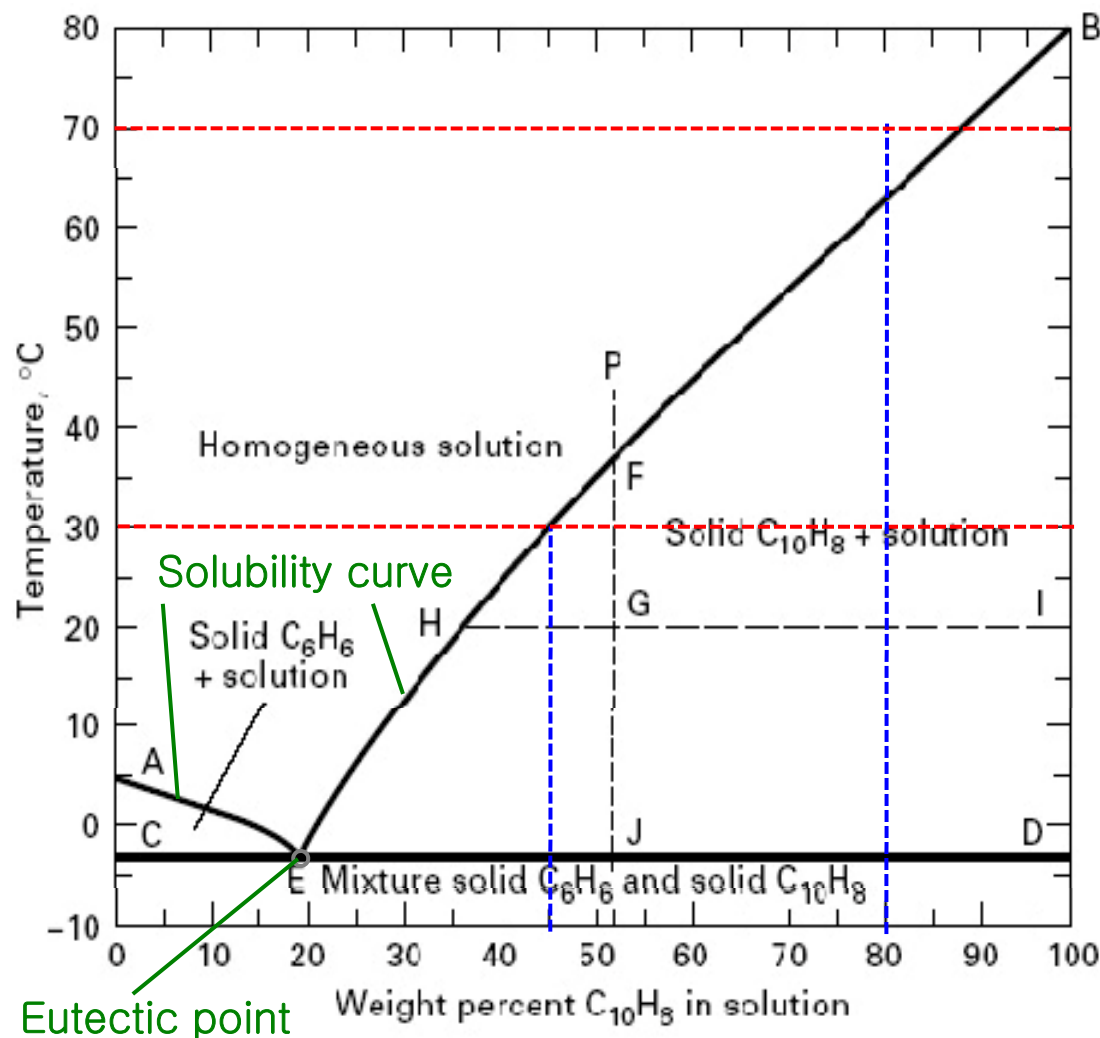
- Applications

- Separation of metal from ore using acid
- Separation of soybean oil from soybean using hexane

# Crystallization



- Crystallization of naphthalene ( $C_{10}H_8$ ) in benzene ( $C_6H_6$ )



8,000 kg/h liquid solution of 80 wt% naphthalene and 20 wt% benzene at 70°C is cooled to 30°C → forming naphthalene crystals

At 30°C, the solubility of naphthalene is 45 wt%.  
By the inverse-lever-arm rule,

$$\frac{\text{kg naphthalene crystals}}{\text{kg original mixture}}$$

$$= \frac{80 - 45}{100 - 45} = 0.636$$

$$= 0.636 \times 8,000 = 5,090 \text{ kg/h}$$

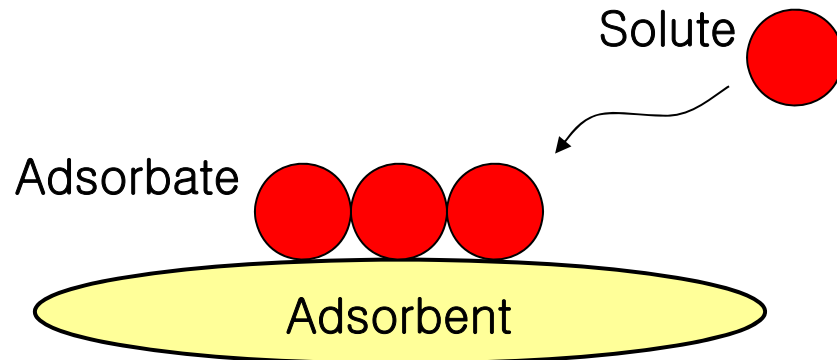
Flow rate of crystals

$$= 0.636 \times 8,000 = 5,090 \text{ kg/h}$$

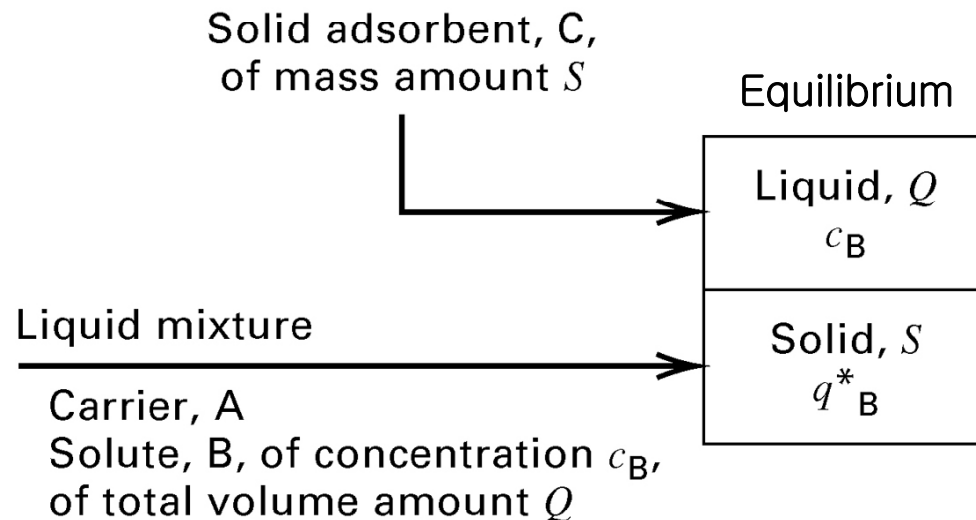
Mother liquor (remaining liquid)

$$= 2,910 \text{ kg/h}$$

# Liquid Adsorption



- The maximum extent of adsorption occurs at equilibrium.

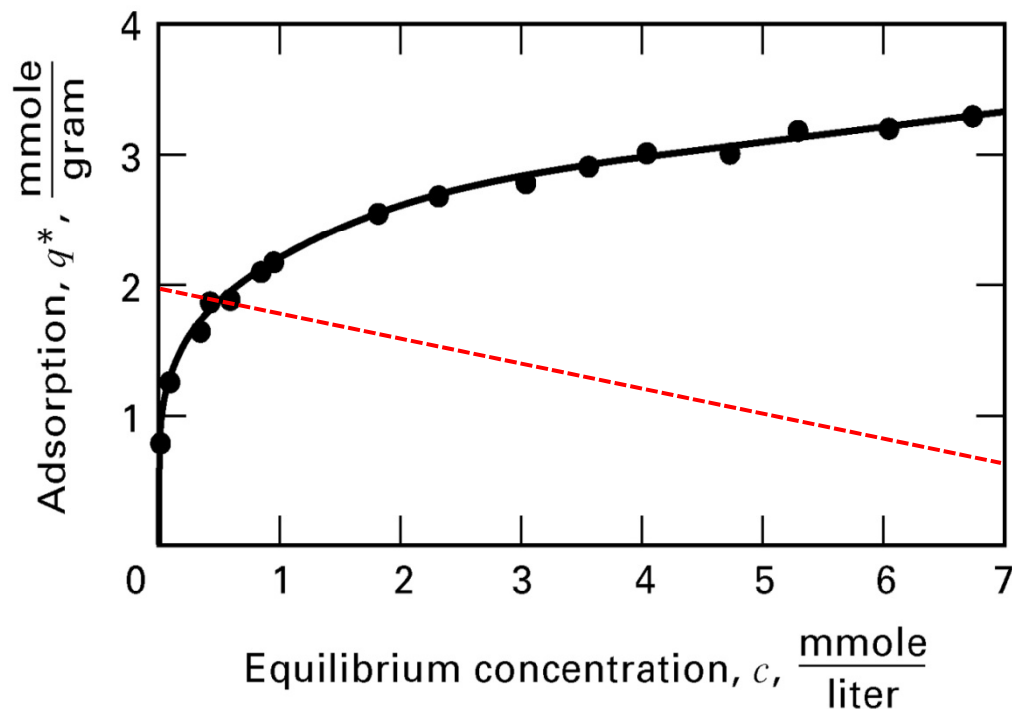


$c_B$ : concentration of solute in the carrier liquid, mol/volume  
 $q_B$ : concentration of adsorbate, mol/mass  
 $Q$ : volume of liquid  
 $S$ : mass of adsorbent

$$c_B^{(F)} Q = c_B Q + q_B^* S \quad \rightarrow \quad q_B^* = -\frac{Q}{S} c_B + c_B^{(F)} \frac{Q}{S}$$

# [Example] Adsorption of Phenol on Activated Carbon

One liter of an aqueous solution containing 0.010 mol of phenol is brought to equilibrium at 20°C with 5 g of activated carbon. Determine the **percent adsorption** of the phenol and **equilibrium concentration** of phenol on carbon.



$$c^{(F)} = 10 \text{ mmol/L}, Q = 1 \text{ L}, S = 5 \text{ g}$$

$$q_B^* = -\frac{Q}{S}c_B + c_B^{(F)}\frac{Q}{S}$$

$$= -\left(\frac{1}{5}\right)c_B + 10\left(\frac{1}{5}\right) = -0.2c_B + 2$$

$$q_B^* = 1.9 \text{ mmol/g}, c_B = 0.57 \text{ mmol/L}$$

The percent adsorption of phenol

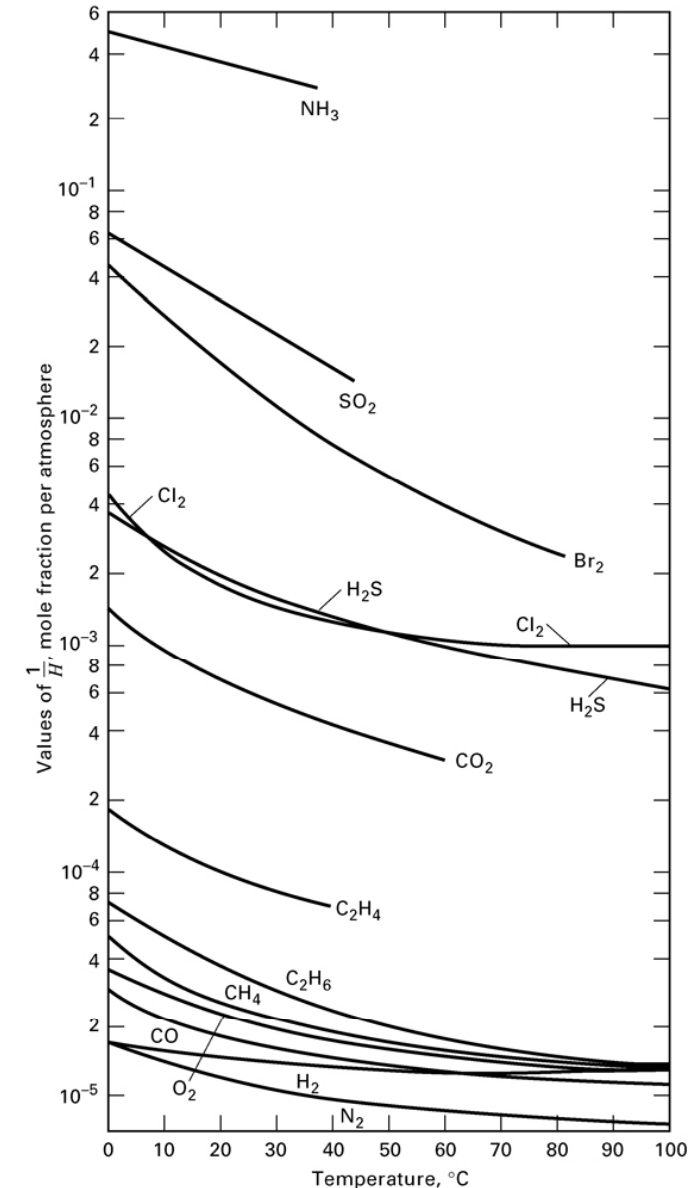
$$\frac{c_B^{(F)} - c_B}{c_B^{(F)}} = \frac{10 - 0.57}{10} = 0.94 \text{ or } 94\%$$

# Gas–Liquid Systems

- **Vapor** : a mixture of species, most or all of which are **condensable**
- **Gas** : a mixture for which the temperature is above the critical temperature of most or all of the species  
→ the components of a gas mixture are **not easily condensed** to a liquid

Estimation of the solubility in water by applying Henry's law

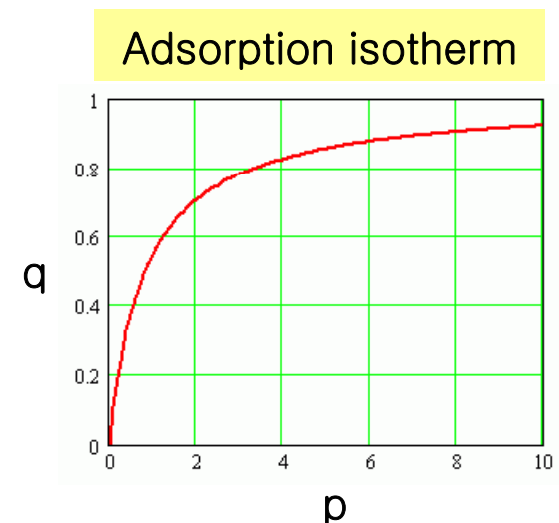
$$x_i = \left( \frac{1}{H_i} \right) y_i P$$





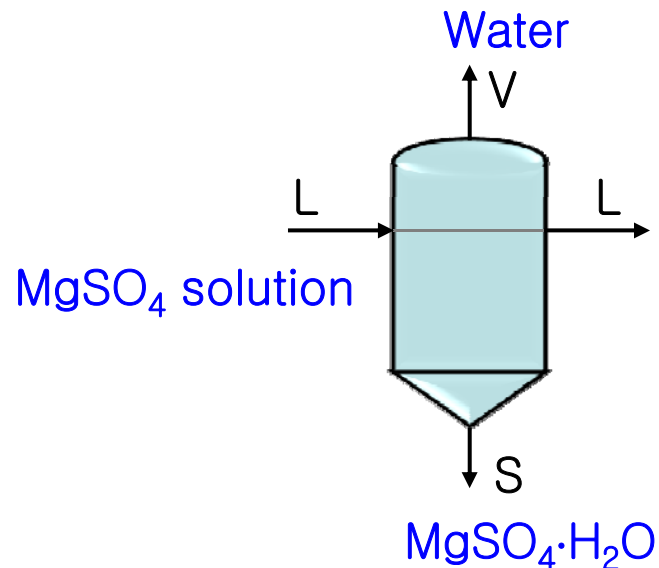
# Gas–Solid Systems

- Sublimation & desublimation
  - **Sublimation**: a **solid** vaporizes into a **gas** phase without passing through a liquid state
  - **Desublimation**: one or more components (solutes) in the **gas** phase are condensed to a **solid** phase without passing through a liquid state
- Gas adsorption
  - One or more components of a gas mixture can be adsorbed on the surface of a solid adsorbent
  - Adsorption isotherm: (partial pressure of solute in the gas) *vs.* (concentration of adsorbate in the solid)



# Vapor–Liquid–Solid Systems

- Example: vacuum evaporative crystallizer
  - The system pressure can be approximated by applying **Raoult's law** to the water in the liquid  $P = P_{H_2O}^s x_{H_2O}$



A 5,000 lb batch of 20 wt% aqueous MgSO<sub>4</sub> solution is fed to a **vacuum, evaporative crystallizer** operating at 160°F. At this temperature, the stable solid phase is the monohydrate, with a MgSO<sub>4</sub> solubility of 36 wt%. 75% of the water is evaporated.

Pounds of water evaporated ?

Feed solution:  $0.2 \times 5,000 = 1,000$  lb MgSO<sub>4</sub>

$5,000 - 1,000 = 4,000$  lb H<sub>2</sub>O

Water evaporated:  $0.75 \times 4,000 = 3,000$  lb H<sub>2</sub>O

# Vapor–Liquid–Liquid Systems

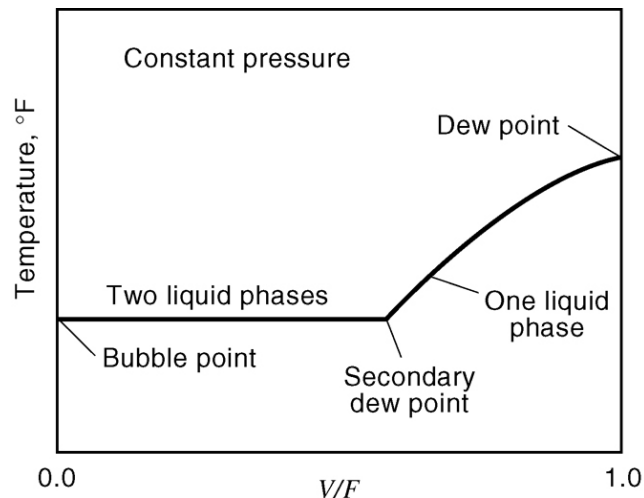
- Example: mixture containing water and hydrocarbons  
→ vapor phase, two liquid phases (HC-rich & water-rich)
- If the solubilities of water in the liquid HC phase and HCs in the water phase are negligible, and the liquid HC phase obeys **Raoult's law**

$$P = P_{H_2O}^s + \sum_{HCs} P_i^s x_i^{(1)}$$

More general cases,

$$P = P_{H_2O}^s + P \sum_{HCs} K_i x_i^{(1)}$$

Only one HC species present



More than one HC species present

