

Lecture 3.

Basic Separation Concepts (2)

[Ch. 1]

- Component Recoveries and Product Purities
 - Split fraction
 - Split ratio
- Separation Power (Separation Factor)
- Selection of Feasible Separation Processes
 - Keller's correlation
 - Technological and use maturities
 - Ease of scale-up

Component Recoveries and Product Purities

- Separation process
 - Conservation of mass
 - For no reaction and continuous, steady–state operation

$$n_i^{(F)} = \sum_{p=1}^N n_i^{(p)} = n_i^{(1)} + n_i^{(2)} + n_i^{(3)} + \dots + n_i^{(N-1)} + n_i^{(N)}$$

$i : 1 \sim C \rightarrow$ Components

$p : 1 \sim N \rightarrow$ Product phases

$F : \text{feed}$

The molar (or mass) flow rate in the feed is equal to the sum of the product molar (or mass) flow rates

Split Fraction and Split Ratio

- Split fraction

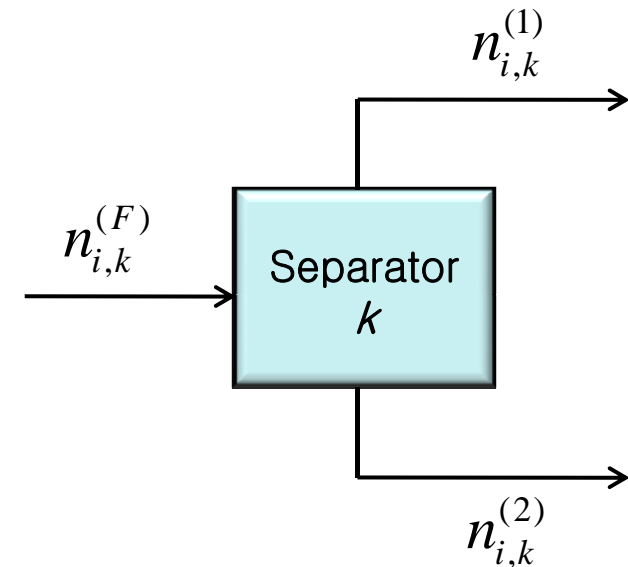
$$SF_{i,k} = \frac{n_{i,k}^{(1)}}{n_{i,k}^{(F)}}$$

Fraction of component i found in the first product

- Split ratio

$$SR_{i,k} = \frac{n_{i,k}^{(1)}}{n_{i,k}^{(2)}} = \frac{SF_{i,k}}{(1 - SF_{i,k})}$$

i : component
 k : separator
 (F) : feed
 (1) : first product (ex: top product)
 (2) : second product (ex : bottom product)



[Example] Hydrocarbon Recovery Process

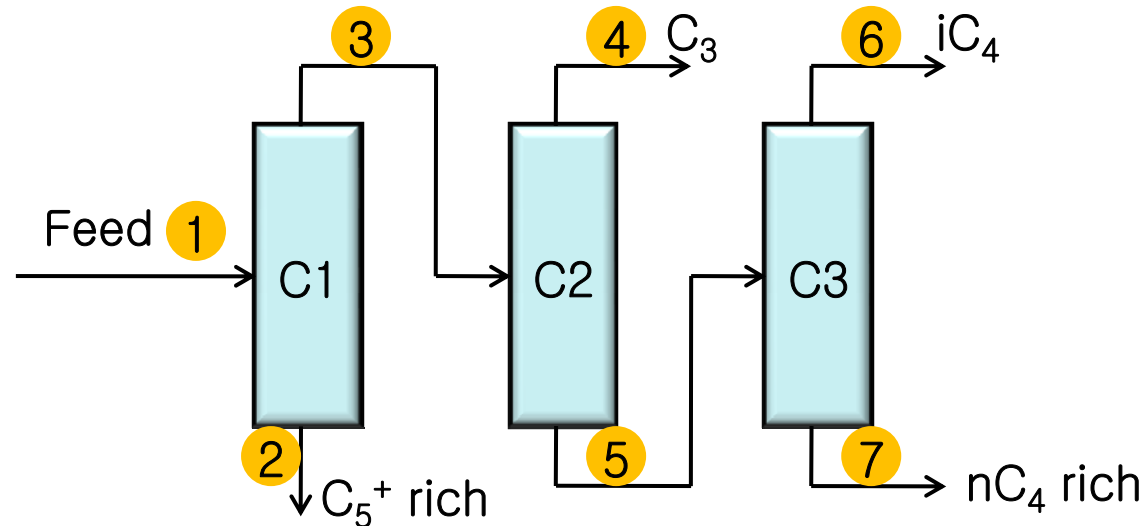


Table 1.5 Operating Material Balance for Hydrocarbon Recovery Process

| Component | lbmol/h in Stream | | | | | | |
|---------------------------------|-------------------|--|-----------------|---------------------|-----------------|----------------------|----------------------------|
| | 1 Feed to C1 | 2 C ₅ ⁺ -rich | 3 Feed to C2 | 4 C ₃ | 5 Feed to C3 | 6 iC ₄ | 7 nC ₄ -rich |
| C ₂ H ₆ | 0.60 | 0.00 | 0.60 | 0.60 | 0.00 | 0.00 | 0.00 |
| C ₃ H ₈ | 57.00 | 0.00 | 57.00 | 54.80 | 2.20 | 2.20 | 0.00 |
| iC ₄ H ₁₀ | 171.80 | 0.10 | 171.70 | 0.60 | 171.10 | 162.50 | 8.60 |
| nC ₄ H ₁₀ | 227.30 | 0.70 | 226.60 | 0.00 | 226.60 | 10.80 | 215.80 |
| iC ₅ H ₁₂ | 40.00 | 11.90 | 28.10 | 0.00 | 28.10 | 0.00 | 28.10 |
| nC ₅ H ₁₂ | 33.60 | 16.10 | 17.50 | 0.00 | 17.50 | 0.00 | 17.50 |
| C ₆ ⁺ | 205.30 | 205.30 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 735.60 | 234.10 | 501.50 | 56.00 | 445.50 | 175.50 | 270.00 |

Product Purity and Specification

Table 1.7 Comparison of Measured Product Purities with Specifications

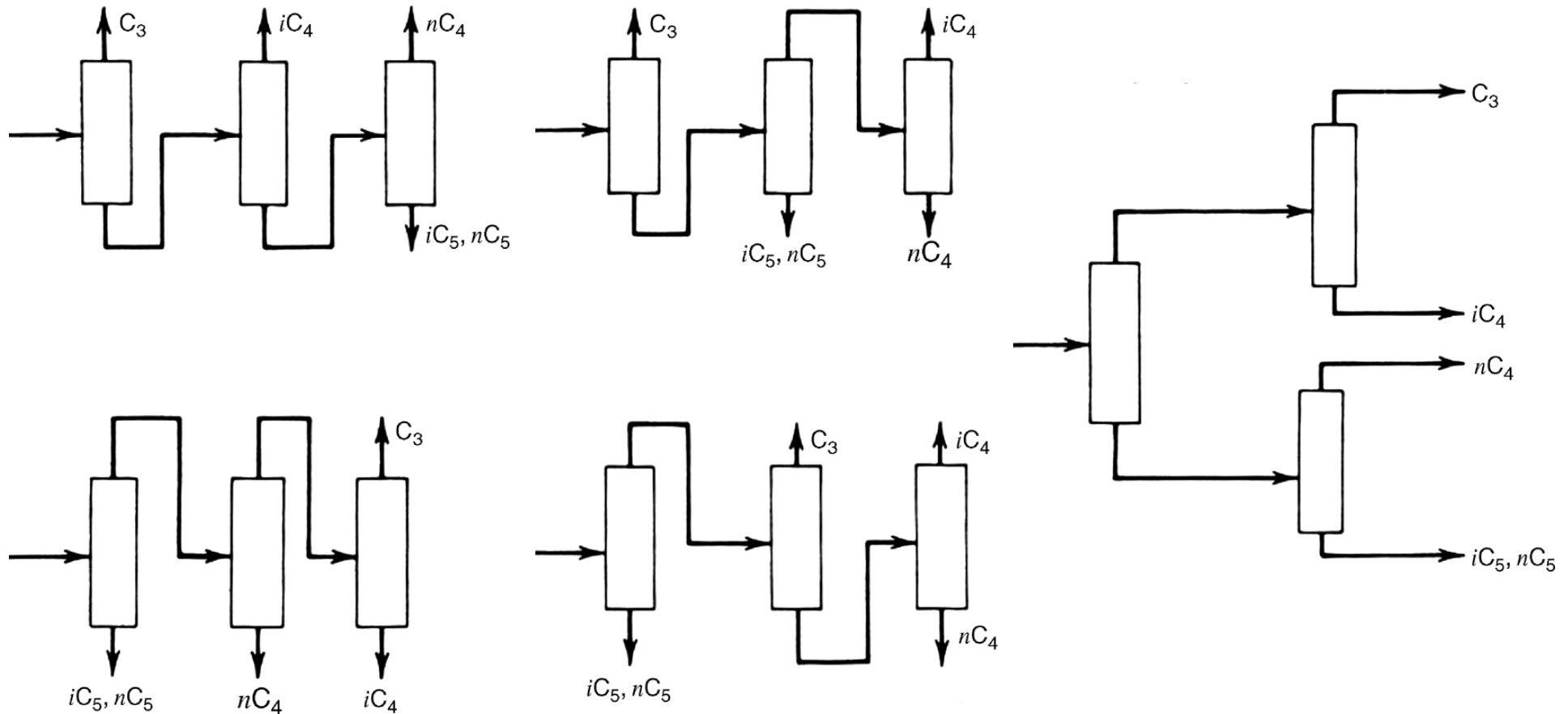
| Component | mol% in Product | | | | | |
|---|-----------------|--------|-----------|--------|---------------|----------|
| | Propane | | Isobutane | | Normal Butane | |
| | Data | Spec | Data | Spec | Data | Spec |
| C ₂ H ₆ | 1.07 | 5 max | 0 | — | 0 | — |
| C ₃ H ₈ | 97.86 | 93 min | 1.25 | 3 max | 0 | 1 max |
| <i>i</i> C ₄ H ₁₀ | 1.07 | 2 max | 92.60 | 92 min | { 83.11 | { 80 min |
| <i>n</i> C ₄ H ₁₀ | 0 | — | 6.15 | 7 max | | |
| C ₅ ⁺ | 0 | — | 0 | — | 16.89 | 20 max |
| Total | 100.00 | | 100.00 | | 100.00 | |

- Product specifications
 - mol%, vol%, wt%
 - ppm (parts per million), ppb (parts per billion)

Separation Sequences

- Hydrocarbon feed : propane (C_3), isobutane (iC_4), n-butane (nC_4), isopentane (iC_5), n-pentane (nC_5)

⇒ Products : C_3 , iC_4 , nC_4 , $iC_5 + nC_5$



Separation Power

- **Separation power** (relative split ratio; separation factor)
 - : relative degree of separation between **two components**, i and j, measured by the compositions of **the two products**

$$SP_{i,j} = \frac{C_i^{(1)} / C_i^{(2)}}{C_j^{(1)} / C_j^{(2)}} = \frac{SR_i}{SR_j} = \frac{SF_i / SF_j}{(1 - SF_i) / (1 - SF_j)}$$

| Key-component split | Column | Separation power |
|---------------------------|--------|------------------|
| nC_4H_{10} / iC_5H_{12} | C1 | 137.1 |
| C_3H_8 / iC_4H_{10} | C2 | 7103 |
| iC_4H_{10} / nC_4H_{10} | C3 | 377.6 |

Achievable SP depends on the number of stages, and the relative thermodynamic and mass transport properties of components

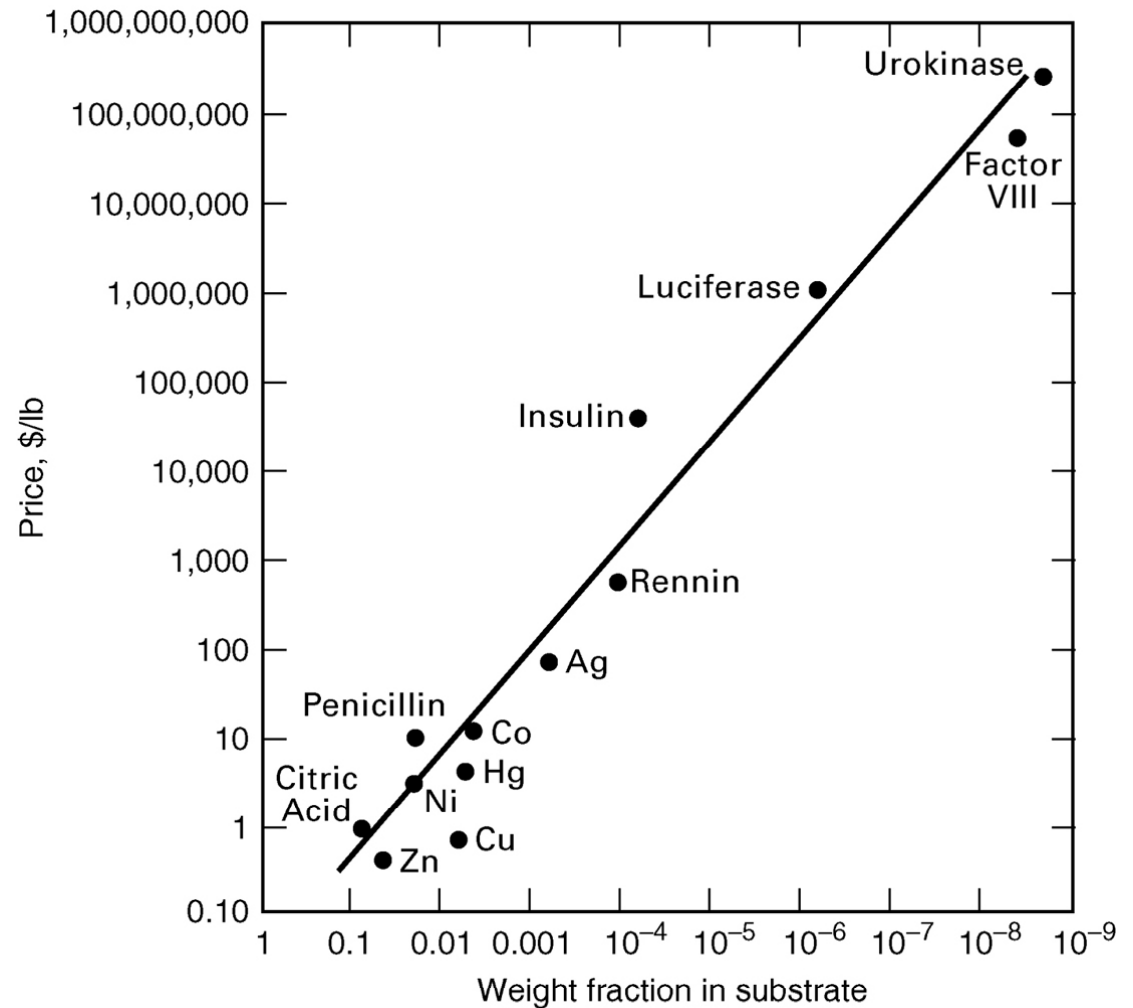
Selection of Feasible Separation

- Selection of a best separation process
 - Selection among a number of feasible candidates
 - A combination of two or more operations may be best
- Factors that influence the selection of feasible separation

| | | |
|--|---|--|
| Feed conditions | <ul style="list-style-type: none"> – Composition – Flow rate – Temperature – Pressure – Phase state | <p>Most important feed conditions</p> <p>Can be altered by pump, compressor, and heat exchangers</p> |
| Product conditions | <ul style="list-style-type: none"> – Required purities – Temperatures – Pressures – Phase states | <p>Most important product conditions</p> |
| Property differences that may be exploited | <ul style="list-style-type: none"> – Molecular – Thermodynamic – Transport | <p>Determine method of separation</p> |
| Characteristics of separation operation | <ul style="list-style-type: none"> – Ease of scale-up – Ease of staging – T, P, phase-state requirements – Physical size limitations – Energy requirements | |

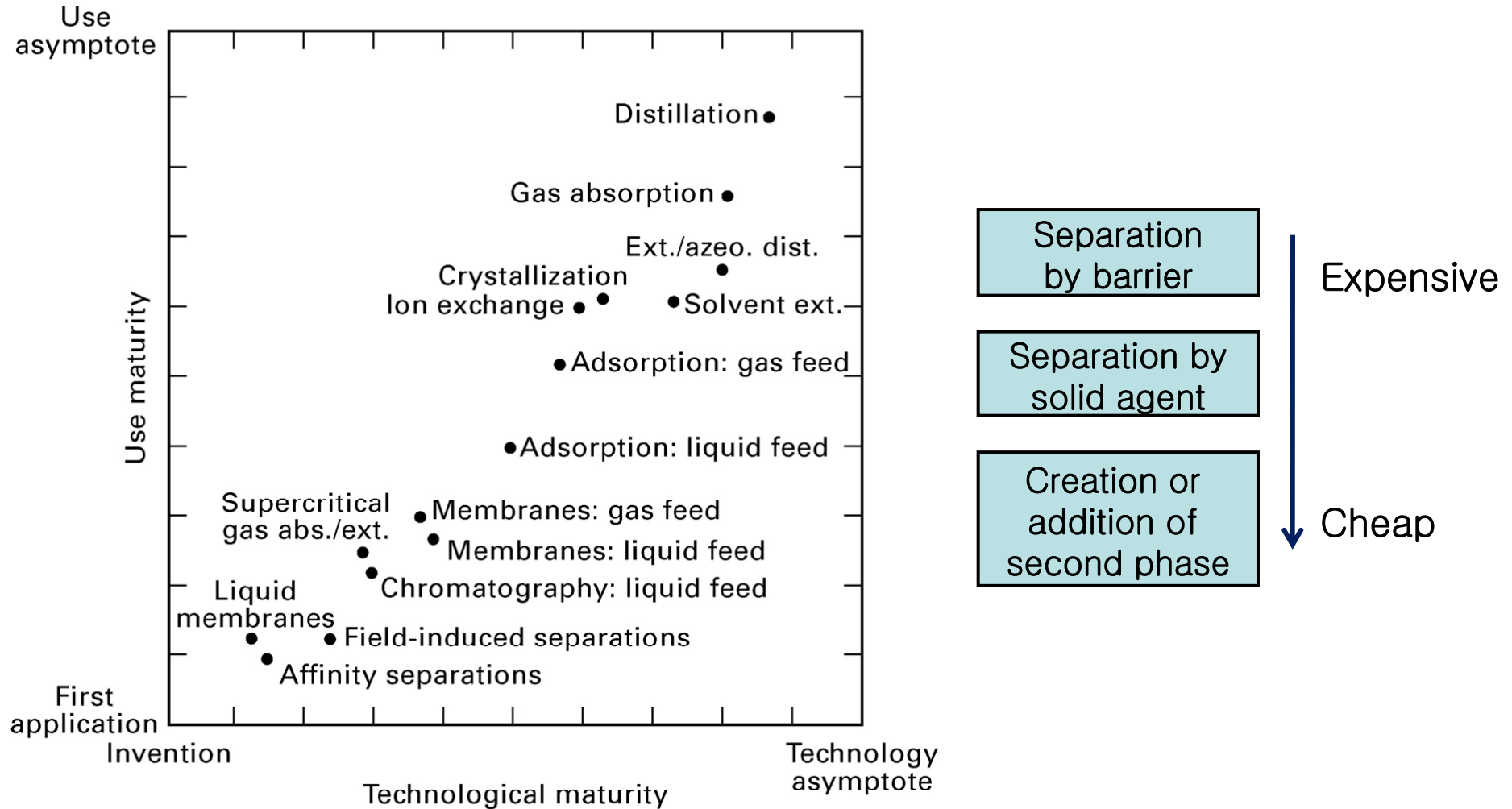
Keller's correlation

- The cost of recovering and purifying a chemical in a mixture can depend strongly on the **concentration**.
- The more dilute the feed, the higher the product price.



Effect of concentration of product in feed material on price

Technological and Use Maturities of Separation Processes



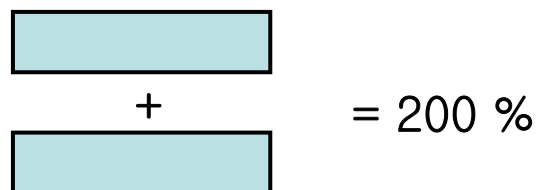
Technological and use maturities of separation processes

Ease of Scale-up

Table 1.10 Ease of Scale-up of the Most Common Separation Operations

| Operation in Decreasing Ease of Scale-up | Ease of Staging | Need for Parallel Units |
|--|---|-----------------------------|
| Distillation | Easy | No need |
| Absorption | Easy | No need |
| Extractive and azeotropic distillation | Easy | No need |
| Liquid-liquid extraction | Easy | Sometimes |
| Membranes | Repressurization required between stages | Almost always |
| Adsorption | Easy | Only for regeneration cycle |
| Crystallization | Not easy | Sometimes |
| Drying | Not convenient | Sometimes |

- If two parallel units are installed, the additional investment is 100%



- The capacity of a single unit can be doubled for an additional investment cost of about 60%

