

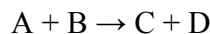
CHME 312, Reaction Engineering, 2011 Spring

Exam II, Open Text (H. Scott Fogler, *Elements of Chemical Reaction Engineering*, 4th Ed.)

Note: For partial credit, please write your answer clearly and legibly.

For better credit, do all algebra and substitute digits, and check final figures carefully.

1. A homogeneous liquid phase second-order irreversible reaction



is to be carried out in a PFR volume of 6.0 ft³. It is proposed that to increase conversion, a CSTR of 100-gal capacity be installed just before the PFR. Calculate the **new conversion**. The values are given by $F_{A0} = F_{B0} = 1.50$ lbmol/hr, Temp. = 300 °F, $v_{A0} = v_{B0} = 4.5$ ft³/hr, and $X = 0.5$. Assume that the reactors are operated isothermally. (50)

Sol)

- Mole Balance on the PFR: $V_{PFR} = F_{A0} \int_0^X \frac{dX}{-r_A}$

- Rate Law: $-r_A = kC_A C_B$

- Stoichiometry: Equal Molar $\Theta_B = 1$

$$C_A = C_{A0}(1 - X), C_B = C_{A0}(1 - X)$$

- Combine

$$V_{PFR} = \frac{F_{A0} X}{k C_{A0}^2 (1 - X)^2}$$

- Evaluate: rearrange to solve for k

$$k = \frac{F_{A0} X}{C_{A0}^2 v_{mix} (1 - X)^2} = \left[\frac{v_0 X}{C_{A0} v_{mix} (1 - X)^2} \right]$$

after mixing

$$v_0 = v_A + v_B = 4.5 \text{ ft}^3/\text{hr} + 4.5 \text{ ft}^3/\text{hr} = 9.0 \text{ ft}^3/\text{hr}$$

$$C_{A0} = \frac{F_{A0}}{v_0} = \frac{1.5 \text{ lbmol/hr}}{9.0 \text{ ft}^3/\text{hr}} = 0.167 \text{ lbmol/ft}^3$$

$$\therefore k = \frac{(9.0 \text{ ft}^3/\text{hr})(0.5)}{(0.167 \text{ lbmol}/\text{ft}^3)(6.0 \text{ ft}^3)((1-0.5))} = 8.98 \frac{\text{ft}^3}{\text{lbmol} \cdot \text{hr}}$$

Place CSTR before original PFR reaction

- Combine : $V_{CSTR} = \frac{F_{A0} X_1}{-r_{A1}}$

- Evaluate

$$V_{CSTR} = \frac{100 \text{ gal} \times 1 \text{ ft}^3}{7.48 \text{ gal}} = 13.37 \text{ ft}^3 = \frac{F_{A0} X_1}{-r_A} = \frac{F_{A0} X_1}{k C_{A0}^2 (1-X_1)^2} = \frac{v_0 X_1}{k C_{A0} (1-X_1)^2}$$

$$V_{CSTR} = \frac{v_0 X_1}{k C_{A0} (1-X_1)^2}$$

$$V_{CSTR} = \frac{v_0 X_1}{k C_{A0} (1-2X_1+X_1^2)}$$

$$V_{CSTR} k C_{A0} - 2V_{CSTR} k C_{A0} X_1 + V_{CSTR} k C_{A0} X_1^2 = v_0 X_1$$

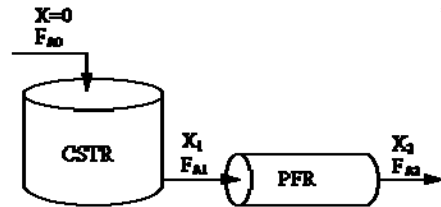
$$X_1^2 - \left(2 + \frac{v_0}{V_{CSTR} k C_{A0}}\right) X_1 + 1 = 0$$

$$X_1 = \frac{\left(2 + \frac{v_0}{V_{CSTR} k C_{A0}}\right) \pm \left[\left(2 + \frac{v_0}{V_{CSTR} k C_{A0}}\right)^2 - 4\right]^{1/2}}{2}$$

where $V_{CSTR} = 13.37 \text{ ft}^3$, $k = 8.98 \frac{\text{ft}^3}{\text{lbmol} \cdot \text{hr}}$, $C_{A0} = 0.167 \text{ lbmol}/\text{ft}^3$, $v_0 = 9.0 \text{ ft}^3/\text{hr}$

$$X_1 = \frac{\left(2 + \frac{9.0}{13.37 \times 8.98 \times 0.167}\right) \pm \left[\left(2 + \frac{9.0}{13.37 \times 8.98 \times 0.167}\right)^2 - 4\right]^{1/2}}{2}$$

$$= 0.52$$



$$V_{PFR} = F_{A0} \int_{X_1}^{X_2} \frac{dX}{kC_{A0}^2(1-X)^2} = \frac{v_0}{kC_{A0}} \int_{X_1}^{X_2} \frac{dX}{(1-X)^2} = \frac{v_0}{kC_{A0}} \left(\frac{1}{1-X_2} - \frac{1}{1-X_1} \right)$$

rearrange :

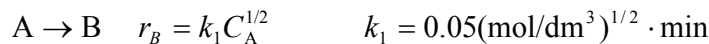
$$\frac{1}{1-X_2} = \frac{1}{1-X_1} + \frac{kC_{A0}V_{PFR}}{v_0}$$

where $X_1 = 0.52$, $V_{PFR} = 6.0 \text{ ft}^3$, $k = 8.98 \frac{\text{ft}^3}{\text{lbmol} \cdot \text{hr}}$, $C_{A0} = 0.167 \text{ lbmol/ft}^3$, $v_0 = 9.0 \text{ ft}^3/\text{hr}$

$$\frac{1}{1-X_2} = \frac{1}{1-0.52} + \frac{(8.98)(0.167)(6.0)}{9.0} = 2.08 + 1 = 3.08$$

$$X_2 = 1 - 1/3.08 = \mathbf{0.675}$$

2. A is converted to B, C, and D according to the following reactions.



Where the k values are specific reaction rates at 27°C . If the reaction is operated at 27°C and 4 atm with pure A entering of volumetric flow rate $10 \text{ dm}^3/\text{min}$. C is desired product and B and D are undesired product and are very costly to separate from B.

(a) Sketch the instantaneous selectivities ($S_{C/B}$, $S_{C/D}$, and $S_{C/BD} = r_C/(r_B + r_D)$) as a function of the concentration of C_A . (20)

$$S_{C/B} = \frac{k_2}{k_1} C_A^{1/2} = 60 C_A^{1/2}$$

$$S_{C/D} = \frac{k_2}{k_3} \frac{1}{C_A} = 1.25 \frac{1}{C_A}$$

$$S_{C/BD} = \frac{k_2 C_A}{k_1 C_A^{1/2} + k_3 C_A^2} = \frac{0.3 C_A}{0.05 C_A^{1/2} + 0.24 C_A^2}$$

- Since only C is desired the selectivity of C over B and D should be the maximum.

$$\lim_{C_A \rightarrow 0} S_{C/BD} = 0 \quad \text{and} \quad \lim_{C_A \rightarrow \infty} S_{C/BD} = 0$$

$$\text{It has maximum value at } \frac{dS_{C/BD}}{dC_A} = 0 \quad \text{or} \quad C_A = \left(\frac{k_1}{2k_2} \right)^{2/3}$$

- (b) What is the **conversion** of A in the first CSTR and how **many** CSTRs will be needed to get over 90% conversion for the process to be profitable? (30)

With k_1 and k_2 values given, $C_A = 0.221$

$$C_{A0} = \frac{P}{RT} = \frac{8 \text{ atm}}{0.082 \frac{\text{dm}^3 \text{ atm}}{\text{mol} \cdot \text{K}} \times 300 \text{ K}} = 0.326 \text{ mol/dm}^3$$

$$V_{CSTR1} = \frac{v_0(C_{A0} - C_A)}{-r_A} = \frac{v_0(C_{A0} - C_A)}{k_1 C_A^{1/2} + k_2 C_A + k_3 C_A^2}$$

$$= \frac{10(0.326 - 0.221)}{(0.05)(0.221)^{1/2} + (0.3)(0.221) + (0.24)(0.221)^2} = \frac{1.05}{0.024 + 0.067 + 0.012} = 10.19 \text{ dm}^3$$

$$X_1 = \frac{(C_{A0} - C_{A1})}{C_{A0}} = \frac{0.326 - 0.221}{0.326} = 0.322$$

$$\text{At 90\% conversion } C_A = 1 - 0.9C_{A0} = 1 - (0.9)(0.326) = 0.033$$

For the 2nd reactor,

$$V_{CSTR2} = \frac{v_0(C_{A1} - C_{A2})}{-r_{A2}} = \frac{v_0(C_{A1} - C_{A2})}{k_1 C_{A2}^{1/2} + k_2 C_{A2} + k_3 C_{A2}^2} = 10.19$$

$$1.019 = \frac{0.221 - C_{A2}}{0.05 C_{A2}^{1/2} + 0.3 C_{A2} + 0.24 C_{A2}^2}$$

By trial & error, $C_{A2} = 0.150$, likewise

$$V_{CSTR3} = \frac{v_0(C_{A2} - C_{A3})}{-r_{A3}} = \frac{v_0(C_{A2} - C_{A3})}{k_1 C_{A3}^{1/2} + k_2 C_{A3} + k_3 C_{A3}^2} = 10.19$$

$$1.019 = \frac{0.150 - C_{A3}}{0.05 C_{A3}^{1/2} + 0.3 C_{A3} + 0.24 C_{A3}^2}$$

By trial & error, $C_{A3} = 0.101$, likewise

$$1.019 = \frac{0.101 - C_{A4}}{0.05 C_{A4}^{1/2} + 0.3 C_{A4} + 0.24 C_{A4}^2}$$

By trial & error, $C_{A4} = 0.066$, likewise

$$1.019 = \frac{0.066 - C_{A5}}{0.05 C_{A5}^{1/2} + 0.3 C_{A5} + 0.24 C_{A5}^2}$$

By trial & error, $C_{A5} = 0.042$, likewise

$$1.019 = \frac{0.042 - C_{A6}}{0.05 C_{A6}^{1/2} + 0.3 C_{A6} + 0.24 C_{A6}^2}$$

By trial & error, $C_{A6} = 0.026 < 0.033$