

## Chapter 2. Single Particles In a Fluid

### 2.1 Motion of Solid Particles in a Fluid

#### 1) Drag Force, $F_D$ :

Net force exerted by the fluid on the spherical particle (diameter  $x$ ) in the direction of flow

$$F_D = C_D \left( \frac{1}{4} x^2 \right) \frac{\rho_f U^2}{2}$$

*Area      Kinetic  
exerted by energy of  
friction unit mass fluid*

where  $C_D$  : Drag coefficient

cf. For pipe flow

$$F_w = f \frac{\rho_f U^2}{2} \rightarrow F_w = f (DL) \frac{\rho_f U^2}{2}$$

where  $f$ : Fanning friction factor

$C_D$  vs.  $Re_p$  - Figure 1.3

$$Re_p = \frac{xU}{\nu}$$

where  $U$  : the relative velocity of particle  
with respect to fluid

- Stokes' law range:  $Re_p < 1$  (creeping flow region)

$$F_D = 3 \pi \mu x U$$

*Stokes' law*

$$= \left( \frac{24}{Re_p} \right) \left( \frac{1}{4} x^2 \right) \frac{\rho_f U^2}{2}$$

$$\therefore C_D = \frac{24}{Re_p}$$

cf.  $f = \frac{16}{Re}$  for pipe flow

- Intermediate range

$$C_D = \frac{24}{Re_p} (1 + 0.15 Re_p^{0.687})$$

or

Table 1.1

- Newton's law range:  $500 < Re_p < 2 \times 10^5$

$$C_D \approx 0.44$$

Newton's law

## 2) Non-continuum Effect for nanoparticles

- Mean-free path of fluid

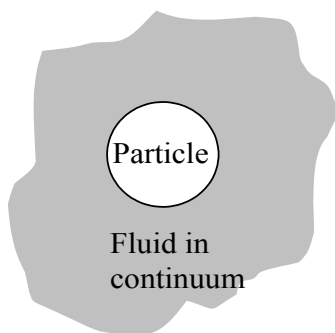
$$= \frac{1}{\sqrt{2} n_m d_m^2}$$

where

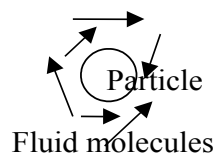
$n_m$  : number concentration of molecules

$d_m$  : diameter of molecules

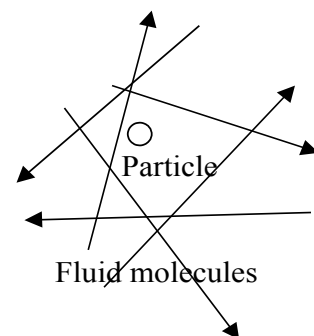
For air at 1 atm and 25°C = 0.0651 μm = 65.1 nm



Continuum regime



transition regime



free-molecule regime

- Knudsen number,  $Kn$

$$Kn = \frac{\lambda}{x}$$

· Continuum regime :  $Kn \sim 0$  ( $< 0.1$ )

· Transition regime :  $Kn \sim 1$  ( $0.1 \sim 10$ )

· Free molecule regime :  $Kn \sim \infty (>10)$

- Drag force corrected for noncontinuum effect

$$F_D = \frac{3}{C_c} \frac{x}{U}$$

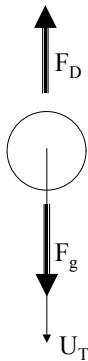
where  $C_c$  : Cunningham correction factor

$$C_c = 1 + Kn[2.34 + 1.05 \exp(-0.39/Kn)]$$

$x, m$	$C_c$
0.01	22.7
0.05	5.06
0.1	2.91
1.0	1.168
10	1.017

In air at 1atm and 25°C

## 2.2 Particle Falling Under Gravity Through a Fluid



The velocity of free falling particle when

$$F_D = F_g - F_B$$

$$\therefore C_D \left( \frac{1}{4} x^2 \right) \frac{\rho_f U^2}{2} = \frac{1}{6} (\rho_p - \rho_f) x^3 g$$

$$\therefore U_T = \left[ \frac{4}{3} \frac{g x}{C_D} \left( \frac{\rho_p - \rho_f}{\rho_f} \right) \right]^{1/2}$$

For Stokes law regime

$$\frac{3}{C_c} \frac{x}{U} = \frac{1}{6} (\rho_p - \rho_f) x^3 g$$

$$\therefore U_T = \frac{(\rho_p - \rho_f) g x^2 C_c}{18}$$

$d_p, m$	$U_T, cm/s^a$
0.1	$8.8 \times 10^{-5}$
0.5	$1.0 \times 10^{-3}$
1.0	$3.5 \times 10^{-3}$
5.0	$7.8 \times 10^{-2}$
10.0	0.31

<sup>a</sup>For unit density particle in air at 1 atm and 25°C

Example. In 1883 the volcano Krakatoa exploded, injecting dust 32km up into the atmosphere. Fallout from this explosion continued for 15 months. If one assumes settling velocity was constant and neglects slip correction, what was the minimum particle size present? Assume particles are rock spheres with a specific gravity of 2.7.

$$\begin{aligned} \therefore U_T &= \frac{(\rho_p - \rho_f) g x^2 C_c}{18} = \frac{2.7 \cdot 980 \cdot x^2 \cdot 1}{18 \cdot 1.81 \cdot 10^{-4}} \\ &= \frac{32 \cdot 10^3 \cdot 10^2}{15 \cdot 30 \cdot 24 \cdot 3600} = 0.0823 \text{ cm/s} \\ \therefore d_p &= 3.19 \text{ m} \end{aligned}$$

Worked Example 1.1

Worked Example 1.4

Worked Example 1.5: Use MathCad

Worked Example 1.6: Use MathCad

\*  $C_D$  for nonspherical particles - Figure 1.3

in terms of sphericity

$$= \frac{\text{surface area of a sphere having the volume of the particle}}{\text{surface area of the particle}}$$

- Dynamic shape factor,  $\chi$

$$\chi \equiv \frac{F_D}{3\pi\mu U x_v}$$

- Equivalent diameters related with terminal settling velocity

• Stokes diameter:

the diameter of the hypothetical sphere having the same terminal settling

velocity

- Aerodynamic diameter:

the diameter of the hypothetical unit-density sphere having the same terminal settling velocity

By definition

$$U_T = \frac{\rho_p x_v^2 g}{18\mu\chi} = \frac{\rho_0 x_a^2 g}{18\mu} = \frac{\rho_p x_s^2 g}{18\mu}$$

or

$$\rho_p \frac{x_v^2}{\chi} = \rho_0 x_a^2 = \rho_p x_s^2$$

Examples

Calculate the aerodynamic diameter(um) for a quartz particle with  $x_e = 20\mu\text{m}$  and

$\rho_p = 2700\text{kg}/\text{m}^3$ . For the quartz particle,  $\chi = 1.36$ .

$$\left[ \frac{2700 \frac{\text{kg}}{\text{m}^3} (20\mu\text{m})^2}{1000 \frac{\text{kg}}{\text{m}^3}} \right]^{\frac{1}{2}} = 3.286 \times 10^{-5} \text{ m}$$

+

$$20\mu\text{m} = 2 \times 10^{-5} \text{ m}$$

## 2.S1 Motion of a Single Particle in an General External Force Field

$$m_p \frac{d\vec{U}}{dt} = - \frac{3}{C_c} x(\vec{U} - \vec{V}) + \sum_i \vec{F}_{ei}$$

where  $\vec{F}_{ei}$ : external force field I

e.g. gravity force, electrical force....

- Its solution gives the motion(trajjectory, displacement) of a single particles with respect to time...

- Steady-state solution gives the migration velocity exerted by the external force fields specified...

External force field	Expression	Migration velocity	Remarks
Gravitational	$m_p g$	$U_T = \frac{(\rho_p - \rho_f) g x^2 C_c}{18}$	Terminal settling velocity
Centrifugal	$F_c = m_p \left(1 - \frac{\rho_f}{\rho_p}\right) r \omega^2$	$U_{cf} = \frac{(\rho_p - \rho_f) x^2 r \omega^2 C_c}{18}$	$r$ : radius of centrifuge $\omega$ : angular velocity
Electrical	$\vec{F} = q\vec{E} = n_e e E$	$U_e = \frac{n_e e E C_c}{3 x}$	$Q$ : charge of particles $E$ : strength of electric field $e$ : charge of electron $n_e$ : number of the units

- Applied to particle classification and separation from fluid

## 2.S2 Inertial Motion of Particles

### 1) Stop Distance

For Stokesian particles

Momentum(force) balance for a single sphere

$$m_p \frac{dU}{dt} = - \frac{3}{C_c} x U$$

Integrating once

$$U = U_0 e^{-t/\tau}$$

$$\text{where } \tau = \frac{m_p C_c}{3 x} = \frac{\rho_p x^2 C_c}{18}$$

relaxation time

Integrating twice

$$x = U_0 \tau (1 - e^{-t/\tau})$$

As  $t \rightarrow \infty$ ,

$$x \sim U_0 \tau = \frac{\rho_p x^2 U_0 C_c}{18} \equiv s$$

stop distance

Example.

What is the stopping distance of a 1- $\mu\text{m}$  aluminum-oxide sphere thrown from a grinding wheel at 9m/s into still air. The particle density is 4000kg/m<sup>3</sup>. Neglect slip correction.

$$\lambda_{\text{vis}} = \frac{4000 \frac{\text{kg}}{\text{m}^3} (1\mu\text{m})^2 9 \frac{\text{m}}{\text{s}}}{18 \cdot 18.1 \cdot 10^{-6} \text{Pa} \cdot \text{s}} = 1.105 \times 10^{-4} \text{ m}$$

$$18.1 \cdot 10^{-6} \text{Pa} \cdot \text{s} = 2.21 \times 10^{-13} \frac{\text{m}^2 \text{ kg}}{\text{s}^2 \text{ m} \cdot \text{s}}$$

$$\text{Re}0 := \frac{1\mu\text{m} \cdot 9 \frac{\text{m}}{\text{s}} \cdot 1.2 \frac{\text{kg}}{\text{m}^3}}{18.1 \cdot 10^{-6} \frac{\text{kg}}{\text{m} \cdot \text{s}}} = 0.597$$

Stokes law can apply.

## 2) Similitude Law for Impaction : Stokesian Particles

If no external force

For  $\text{Re} < 1$

Force balance around a particle (equation of particle motion)

$$m_p \frac{d\vec{U}}{dt} = -3 \quad x(\vec{U} - \vec{U}_f)$$

Defining dimensionless variables

$$\vec{U}_1 \equiv \frac{\vec{U}}{U}, \quad \vec{U}_f \equiv \frac{\vec{U}_f}{U} \quad \text{and} \quad \tau \equiv \frac{tU}{L}$$

where  $U$ ,  $L$ : characteristic velocity and length of the system

Substituting

$$m_p \frac{d(\vec{U}_1 U)}{d(\frac{L}{U})} = -3 \quad x(\vec{U}_1 U - \vec{U}_f U)$$

$$\therefore \text{St} \frac{d\vec{U}_1}{d\tau} = -(\vec{U}_1 - \vec{U}_f)$$

$$\text{where } \text{St} \equiv \frac{m_p U}{3 \quad xL} = \frac{\frac{\rho}{6} x^3 U}{3 \quad xL} = \frac{\rho x^2 U}{18 \quad L} = \frac{U}{L} \equiv \frac{\text{particle persistence}}{\text{size of obstacle}}$$

Stokes number

In terms of displacement  $\vec{U} = \frac{d\vec{r}}{dt}$

where  $\vec{r}$ : displacement vector ( $r_1 \equiv \frac{\vec{r}}{L}$ )

$$\rightarrow \vec{U}_1 U = \frac{d(\vec{r}_1 L)}{d(\frac{\theta L}{U})} \rightarrow \vec{U}_1 = \frac{d\vec{r}_1}{d\theta}, \quad \text{and} \quad \frac{d\vec{U}_1}{d\theta} = \frac{d^2 \vec{r}_1}{d\theta^2}$$





- Random wiggling motion of particles by collision of fluid molecules on them
- Important for motion of nanoparticles
- Stochastic vs. deterministic
- Including Brownian motion term in the motion equation

$$m_p \frac{d\vec{U}}{dt} = - \frac{3}{C_c} x(\vec{U} - \vec{U}_f) + \sum_i \vec{F}_{ei} + m_p \alpha(t)$$

Langevin equation...

where  $\alpha(t)$ : random acceleration caused by bombardment by molecules

For pure Brownian motion, all the  $\vec{F}_{ei} = 0$  and  $\vec{U}_f = 0$

The mean square displacement of the Brownian motion  $(\bar{s}^2)^{1/2}$  is given

$$(\bar{x}^2) = (\bar{y}^2) = (\bar{z}^2) = \frac{2kTC_c t}{3\pi\mu x} \quad (1)$$

Brownian Diffusion :

- Particle migration due to concentration gradient by Brownian motion

$$\vec{J} = - D_p \vec{\nabla} C$$

1st Fick's law

where  $D_p$  : diffusion coefficient of particles  $cm^2/s$

- Phenomenological expression with collective properties

- The material balance caused by Brownian motion

$$\frac{\partial C}{\partial t} = - \nabla \cdot \vec{J} = D_p \nabla^2 C$$

2nd Fick's law

$C$  : particle concentration by number or mass

The solution gives

$$(\bar{x}^2) = (\bar{y}^2) = (\bar{z}^2) = 2D_p t \quad (2)$$

From (1) and (2)

$$D_p = \frac{kTC_c}{3\pi\mu x}$$

Stokes-Einstein relation

**Example**

Calculate the diffusion coefficient for a 1-um particle at standard conditions.

$$Kn = \frac{0.066 \cdot \mu\text{m}}{0.1 \mu\text{m}}$$

$$Cc := 1 + Kn \left( 2.34 + 1.05 \exp\left(\frac{-0.39}{Kn}\right) \right) = 2.928$$

$$k := 1.38 \cdot 10^{-23} \frac{\text{J}}{\text{K}} \quad T := 293\text{K}$$

$$x := 1 \mu\text{m} \quad \mu := 18.1 \cdot 10^{-6} \text{Pa} \cdot \text{s}$$

$$D := \frac{k \cdot T \cdot Cc}{3\pi \mu \cdot x} = 6.941 \times 10^{-11} \frac{\text{m}^2}{\text{s}}$$

Diffusion Coefficient of Unit-density sphere at 20°C in air

액체분자의 확산계수  $10^5 \text{cm}^2/\text{s}$  정도

Particle diameter, m	Diffusion coefficient, $D_p(\text{cm}^2/\text{s})$
0.00037(air molecule)	0.19
0.01	$5.2 \times 10^{-4}$
0.1	$6.7 \times 10^{-6}$
1.0	$2.7 \times 10^{-7}$
10	$2.4 \times 10^{-8}$

- Determines behavior of nanoparticles:

Brownian coagulation

Brownian deposition...

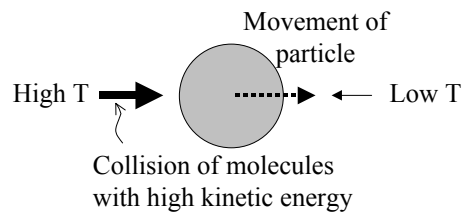
- Applied to diffusion batteries

dynamic light scattering(photon correlation spectroscopy)

: Brown 운동하는 입자의 빛산란을 추적하여 입자크기 측정

**2) Thermophoresis**

- Discovered by Tyndall in 1870



실제 예 : radiator의 벽이나 인근 벽에 먼지가 쓸지 않는 현상  
 담배연기가 차가운 벽 또는 창문 쪽으로 이동해 가는 현상  
 차가운 쪽에 면한 벽이 먼저 더러워지는 현상

Thermophoretic force and velocity

- In free molecular regime

$$\vec{F}_{th} = -p \cdot x^2 \frac{\vec{\nabla} T}{T}$$

Waldmann and Schmidt(1966)

From  $\vec{F}_{th} = \vec{F}_D$  in Stokes' regime

$$\therefore \vec{U}_{th} = - \frac{3 \vec{\nabla} T}{4 \left(1 + \frac{8}{3}\right) T} = \sim 0.55 \frac{\vec{\nabla} T}{T}$$

- independent of  $x$

- Correction for continuum fluid-particle interaction

$$\vec{F}_{th} = \frac{-9}{2} \frac{k_G H \vec{\nabla} T}{k_p T}$$

Brock(1962)

$$H \sim \frac{1}{1 + 6Kn} \frac{\frac{k_G}{k_p} + 4.4Kn}{1 + 2 \frac{k_G}{k_p} + 8.8Kn}$$

$$\therefore \vec{U}_{th} = \frac{-3}{2} \frac{C_e H \vec{\nabla} T}{k_p T}$$

Terminal settling and thermophoretic velocities in a temperature gradient of 1°C/cm at 293K

<sup>a</sup>  $K_p = 10k_a$

Particle diameter( m)	Terminal settling velocity(m/s)	Thermophoretic velocities in a temperature gradient of 1°C/cm at 293K <sup>a</sup>
0.01	$6.7 \times 10^{-8}$	$2.8 \times 10^{-6}$
0.1	$8.6 \times 10^{-7}$	$2.0 \times 10^{-6}$
1.0	$3.5 \times 10^{-5}$	$1.3 \times 10^{-6}$
10.0	$3.1 \times 10^{-3}$	$7.8 \times 10^{-7}$

-  $U_{th}$ : independent of particle size

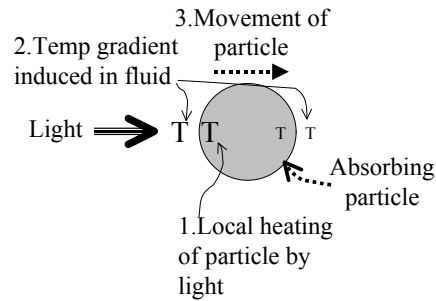
Applications

- Particle sampling: dust collection in UK mines

- Suppression of particle deposition of particles in fine industries and hospitals

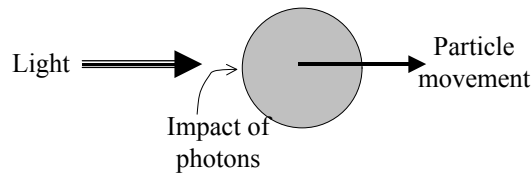
### 3) Phoresis by Light

#### Photophoresis



- Where to be heated depends on the refractive index of the particle  
e.g. Movement of submicron particles in the upper atmosphere

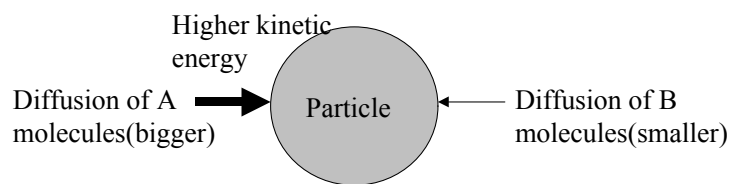
#### Radiation pressure



- e.g. tails of comet, laser-lift of particles

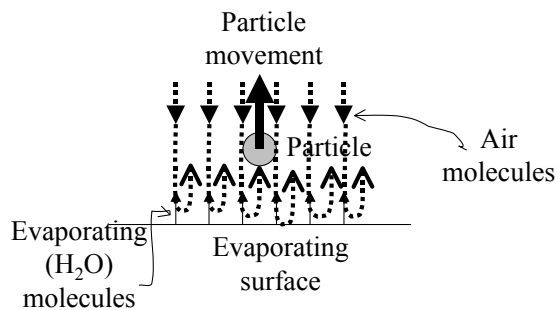
### 4) Diffusion of medium

#### Diffusiophoresis

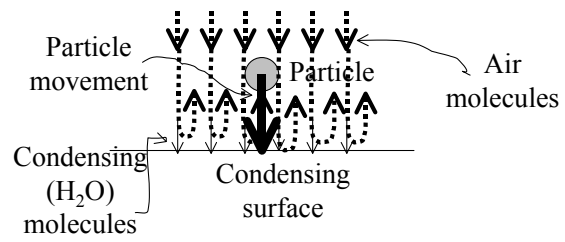


#### Stefan flow

- For evaporating surface



- For condensing surface



*e.g. Venturi scrubber*