Chapter 14 and 15 Polymer viscoelasticity

(Ref. John.D.Ferry, Viscoelastic Properties of polymers, John Wiley(1980))

• Hooke's Law :

=Y с

the strain ε is proportional to the stress , Y is Young's modulus(tensile strength)



(b)



- shear strain : $\gamma = \frac{dx}{dy}$ (dimensionless)
- shear rate : $\dot{\gamma} = \frac{d}{dt}(\gamma) = \frac{d}{dt}(\frac{dx}{dy}) = \frac{d}{dy}(\frac{dx}{dt}) = \frac{du}{dy}$ (time⁻¹)
 - an alternate definition of the shear rate is the velocity gradient du/dy.

• shear stress : =
$$\frac{F(in \ x \ direction)}{A(in \ y \ direction)} \left(\frac{force}{length^2}\right)$$

- viscosity : $\eta \equiv \frac{\tau}{\cdot}$
- \circ Relations between and $\overset{\bullet}{\gamma}$ Flow curves.
- Newton's law : shear stress is linearly proportional to the shear rate, the proportionality constant being the viscosity .

=
$$\gamma$$
 (= dyne sec/cm²)

Taking logarithm :

 $\log = \log + \log \frac{1}{\gamma}$

• = γ^n

taking logarithm : log = log + $\underline{n} \log \gamma$



(a) n = 1 (7)): Newtonian flow

(= constant)

- for small molecules (ex : silicone polymer)
- the structure, the resistance to flow does not change with the intensity of shearing
- (b) n < 1 : pseudoplastic flow (shear thinning)

decreases with increase of $\dot{\gamma}$: = f($\dot{\gamma}$)

(e.g.) polymer melts and solutions

- resistance to flow decreases with the intensity of shearing.

(c) n > 1: dilatant flow (shear – thickening)

increases with the increase of γ

(e.g.) slurries, suspension()

- resistance to flow increases with the intensity of shearing

• Bingham plastic

$$\tau$$
 (ex)emulsion ()

- three types of fluid
- (a) Newtonian fluid

(b) Non-newtonian fluid

$\begin{pmatrix} pseudoplastic flow \\ dilatan t flow \end{pmatrix}$

-these two fluids, though shear dependent, are time independent; (constant) shear rate stress가 maintain , the same viscosity will be observed at equilibrium.

- Time dependent behavior :
 - (a) Rheopetic
 - (b) Thixotropic
 - (a) Rheopetic fluid when sheared at a constant rate or stress, the viscosity will increase over a period of time.
 (e.g.) muds
- (b) Thixotropic fluid when sheared at a constant rate or stress, the viscosity will decrease over a period of time.
 (e.g.) ketchup, paint





- Fig. Flow curves for time-dependent fluids under continuously increasing and then decreasing shear.
- the system is not reversible and that is due to degradation or crosslinking of the polymer when in the viscometer for long periods of time, particularly at elevated temperatures.
- but for chemically stable polymer melts or solutions, the equilibrium viscous properties are time independent.
- Polymer Melts and Solutions
- (a) at low shear rates, a 'lower Newtonian"

```
region is reached with a so - called zero - shear viscosity (<sub>0</sub>).
```

- (b) In intermediate range of shear rates, the material is pseudoplastic.
- (c) at very high shear rates, upper Newtonian "region with viscosity η_{∞} is attained.



Fig. Generalized flow properties for polymer melts and solutions

- (a) The molecules are in their most random and highly entangled state, and have their greatest resistance to slippage(flow).
- (b) The molecules begin to unentangle and align in the shear field, reducing their resistance to flow.
- (c) Pretty much completely untangled and aligned, and reach a state of minimum resistance to flow. Sometimes mechanical degradation.

1

Quantitative representation of flow behavior

- for purely viscos non -Newtonian flow

$$\tau = K(\gamma)^n$$
 (power law)

where K=consistency (depend on n) n=flow index

 $\tau = K(\gamma)^n$ $(\gamma)^n$ dimension

$$\tau = K \left| \frac{\bullet}{\gamma} \right|^{n-1} \cdot \frac{\bullet}{\gamma}$$

(K has the usual viscosity units)

when n=1: Newton's law

n<1: Pseudoplastic fluid

n >1: Dilatant fluid

Melt flow in screw extruder channel

 $10 < \gamma < 10^2$

• Melt flow in injection molding

$$10^2 < \gamma < 10^3$$

n : PE 0.3~0.6
 PP 0.3~0.4
 PVC 0.2~0.5
 Nylon 0.6~0.9

(ex) Determine the equation relating viscosity to shear rate for a power-law fluid.

(sol)
$$\eta = \frac{\tau}{\gamma} = \frac{K(\gamma)}{\gamma} = K(\gamma)^{n-1}$$

Temperature dependence of flow properties

$$\eta = f(\tau,T)$$
 or $\eta = f'(\gamma,T)$

• zero-shear viscisity,
$$\eta_{\scriptscriptstyle 0}$$
 = $Ae^{^{E/RT}}$

E=flow activation energy

•
$$\eta_0 = Be^{E/RT}$$
 (τ :constant)

•
$$\eta_0 = Be^{E/RT}$$
 ((γ): constant)

A more general expression for the variation of $\,\eta_{_0}\,$ with temperature:

$$\log \frac{\eta_0(T)}{\eta_0(T_g)} = -\frac{17.44(T-T_g)}{51.6 + (T-T_g)}$$

William - Landell - Ferry (WLF) equation

-good for a wide variety of polymers in the temperature range of T_g to $T_g + 100\,^{\it o}C$

Influence of molecular weight on Flow Properties.

- by empirical equation

$$\eta_{_0} \propto (M_{_W})^1$$
 for $M_{_W} < M_{_W}$

$$\eta_{0} \propto (\bar{M}_{w})^{3.4}$$
 for $\bar{M}_{w} > \bar{M}_{wc}$

where \bar{M}_{wc} is a critical molecular weight.

 M_{wc} depends on the temp and polymer type, but most commercial polymers are well above \bar{M}_{wc} .

 $\overline{M}_{wc} \approx 4000 \sim 50000 (g/mole)$ -entanglement7 M.W.(500~600 carbon atom)

 $p.s = \bar{M}_{wc}$ (40000)



Fig. The effect of molecular weight on viscosity.

MWD (Molecular weight distribution) effects on η



Broad MWD→

chain braching effects on η .

Short branch - η . decrease

Longbranch - η . Increase (entanglement γ)