Chapter 14 and 15 Polymer viscoelasticity

(Ref. John.D.Ferry, Viscoelastic Properties of polymers, John Wiley(1980))

• Hooke's Law :

 $= Y \epsilon$

the strain ϵ is proportional to the stress, Y is Young's modulus(tensile strength)

(b)

- shear strain : $\gamma = \frac{dx}{dy}$ (dimensionless)
- shear rate : $\dot{\gamma} = \frac{d}{dt}(\gamma) = \frac{d}{dt}(\gamma)$ $\frac{dx}{dy}$) = $\frac{d}{dy}$ ($\frac{dx}{dt}$) = $\frac{du}{dy}$ (time⁻¹)
- an alternate definition of the shear rate is the velocity gradient du/dy.

• shear stress :
$$
= \frac{F(in x \text{ direction})}{A(in y \text{ direction})} \left(\frac{force}{length^2} \right)
$$

- viscosity : $\eta = \frac{v}{\cdot}$ γ $\eta \equiv \frac{\tau}{2}$
- \circ Relations between and $\dot{\gamma}$ - Flow curves.
- Newton's law : shear stress is linearly proportional to the shear rate, the proportionality constant being the viscosity.

$$
=\dot{\gamma}
$$
 (= dyne sec/cm²)

Taking logarithm :

 \log = \log + $\log \frac{1}{\gamma}$

$$
z
$$

Bingham Plastic
Newtonian
Pseudoplastic
 \overrightarrow{r}

 \bullet = \bullet *n* • γ

taking logarithm : log = log + $\frac{\cdot}{n}$ log $\frac{\cdot}{\gamma}$

- (a) $n = 1$ () : Newtonian flow $($ = constant)
- for small molecules (ex : silicone polymer)
- the structure, the resistance to flow does not change with the intensity of shearing
- (b) $n < 1$: pseudoplastic flow (shear thinning)

decreases with increase of $\dot{\gamma}$: = f($\dot{\gamma}$)

(e.g.) polymer melts and solutions

- resistance to flow decreases with the intensity of shearing.

(c) $n > 1$: dilatant flow (shear – thickening)

increases with the increase of \dot{y}

 $(e.g.)$ slurries, suspension $($)

- resistance to flow increases with the intensity of shearing

• Bingham plastic

$$
\tau_{\bullet} \left\{\right| \qquad \qquad \text{(ex)emulsion (}
$$

- three types of fluid
- (a) Newtonian fluid
	-

(b) Non-newtonian fluid $\begin{bmatrix} P\text{scm} \\ \text{dilat} \\ \text{dilat} \end{bmatrix}$ $\overline{}$ \setminus ſ *dila t flow pseudoplasticflow* tan

-these two fluids, though shear dependent, are time independent ; (constant) shear rate stress maintain , the same viscosity will be observed at equilibrium.

 $\bigg)$ \setminus

- Time dependent behavior :
	- (a) Rheopetic
	- (b) Thixotropic
- (a) Rheopetic fluid when sheared at a constant rate or stress, the viscosity will increase over a period of time. (e.g.) muds
- (b) Thixotropic fluid when sheared at a constant rate or stress, the viscosity will decrease over a period of time. (e.g.) ketchup, paint

- Fig. Flow curves for time-dependent fluids under continuously increasing and then decreasing shear.
- the system is not reversible and that is due to degradation or crosslinking of the polymer when in the viscometer for long periods of time, particularly at elevated temperatures.
- but for chemically stable polymer melts or solutions, the equilibrium viscous properties are time independent.
- Polymer Melts and Solutions
- (a) at low shear rates, a "lower Newtonian"

region is reached with a so – called zero – shear viscosity $\binom{1}{0}$.

- (b) In intermediate range of shear rates, the material is pseudoplastic.
- (c) at very high shear rates, 'upper Newtonian" region with viscosity η_{∞} is attained.

Fig. Generalized flow properties for polymer melts and solutions

- (a)The molecules are in their most random and highly entangled state, and have their greatest resistance to slippage(flow).
- (b) The molecules begin to unentangle and align in the shear field, reducing their resistance to flow.
- (c)Pretty much completely untangled and aligned, and reach a state of minimum resistance to flow.Sometimes mechanical degradation.

Quantitative representation of flow behavior

for purely viscos non-Newtonian flow

$$
\tau = K(\gamma)^n \qquad \text{(power law)}
$$

where K=consistency (depend on n) n=flow index

 $\tau = K(\gamma)^n$ (*γ*)^{*n*} dimension and the state \sim

$$
\tau = K \begin{bmatrix} \bullet \\ \gamma \\ \gamma \end{bmatrix}^{n-1} \cdot \gamma
$$

(K has the usual viscosity units)

when n=1: Newton's law

n<1: Pseudoplastic fluid

n>1: Dilatant fluid

• Melt flow in screw extruder channel

 $10 < \gamma < 10^2$

▪ Melt flow in injection molding

$$
10^2 < \gamma < 10^3
$$

 \blacksquare n : PE 0.3~0.6 PP 0.3~0.4 PVC 0.2~0.5 Nylon 0.6~0.9

(ex) Determine the equation relating viscosity to shear rate for a power-law fluid.

$$
\text{(sol)} \quad \eta = \frac{\tau}{\gamma} = \frac{K(\gamma)}{\gamma} = K(\gamma)^{n-1}
$$
\n
$$
\gamma = \frac{\tau}{\gamma}
$$

Temperature dependence of flow properties

$$
\eta = f(\tau, T) \text{ or } \eta = f'(\gamma, T)
$$

• zero-shear viscisity, $\eta_0 = Ae^{E/RT}$

E=flow activation energy

- *n*₀ = $Be^{E/RT}$ (τ : constant)
- *n*₀ = $Be^{E/RT}$ ((γ): constant)

A more general expression for the variation of $\eta_{\scriptscriptstyle 0}^{\scriptscriptstyle\prime}$ with temperature:

$$
\log \frac{\eta_{0}(T)}{\eta_{0}(T_{g})} = -\frac{17.44(T - T_{g})}{51.6 + (T - T_{g})}
$$

William-Landell-Ferry(WLF)equation

- good for a wide variety of polymers in the temperature range of T_g to $T_{\rm g}$ +100 oC

Influence of molecular weight on Flow Properties.

- by empirical equation

$$
\eta_{0} \propto (\bar{M}_{w})^{1} \quad \text{for } \bar{M}_{w} < \bar{M}_{wc}
$$

$$
\eta_{0} \propto (\bar{M}_{w})^{3.4} \quad \text{for} \quad \bar{M}_{w} > \bar{M}_{wc}
$$

where \overline{M}_{wc} is a critical molecular weight.

 \overline{M}_{wc} depends on the temp and polymer type, but most commercial polymers are well above \overline{M}_{wc} .

 \overline{M}_{wc} ≈ 4000~50000(g/mole) - entanglement M.W.(500~600 carbon atom)

 $p.s = \overline{M}_{wc}(40000)$

Fig. The effect of molecular weight on viscosity.

MWD(Molecular weight distribution) effects on η

Broad MWD \longrightarrow

chain braching effects on η .

Short branch - η . decrease

Longbranch - η . Increase(entanglement)