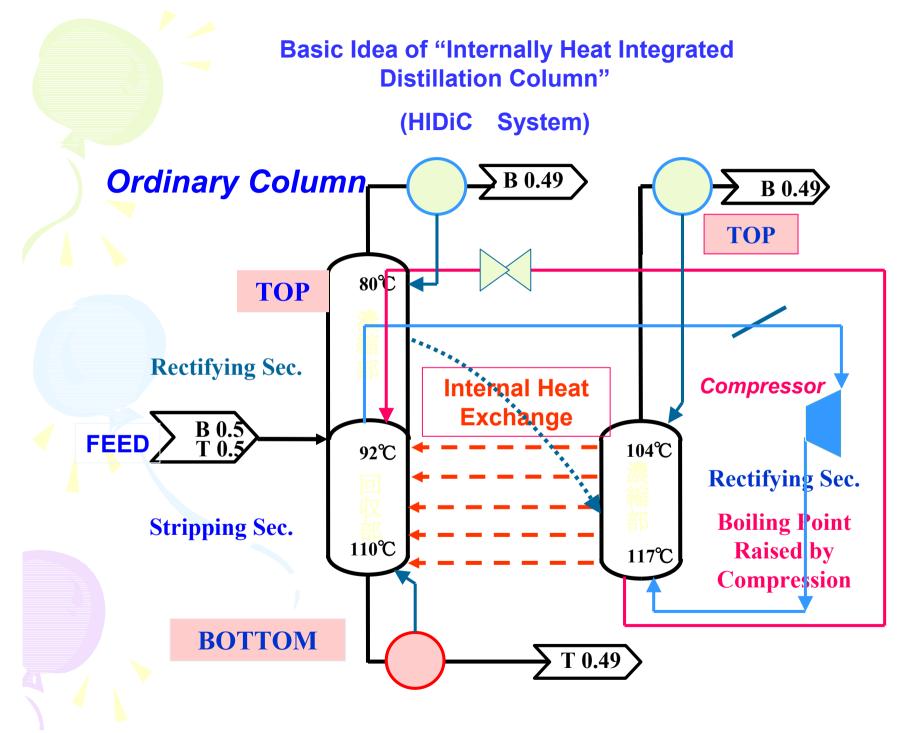
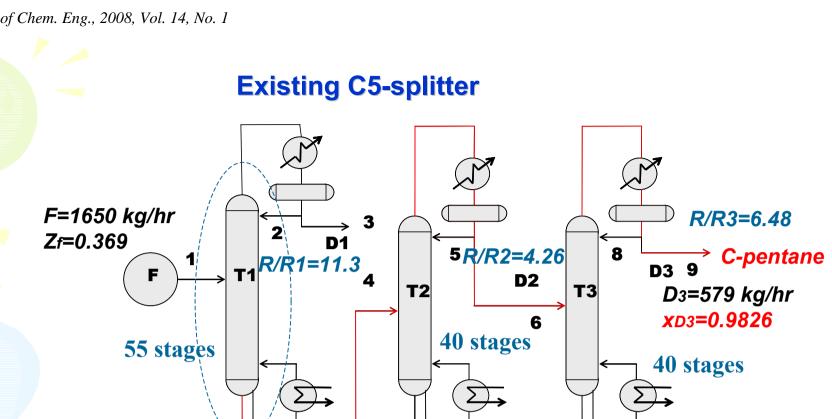
Challenging Intensification of Petro-industrial Distillation Processes by a New Internal Heat Integration Method

Kunio Kataoka* Kansai Chemical Engineering Co., Ltd, 2-9-7 Minami-nanamatsu-cho, Amagasaki 660-0053, Japan (kataoka@kce.co.jp)



2002-2007 NEDO Project Title: R&D of Heat Integrated Distillation Technology for Prevention Against Global Warming

Project Team National Institute of Advanced Industrial Science and Technology Maruzen Petrochemical Co., Ltd Kimura Chemical Plants Co., Ltd Kansai Chemical Engineering Co., Ltd



Purification of c-pentane from mixed gasoline

 Table 1 Feed Composition

W2

W3

10

7↓

W1

	u c	Component	Wt%	Component	Wt%
~	column	n-butane	0.04	2-methylpentane	13.57
tom		i-pentane	1.80	3-methylpentane	4.71
To the bottom	first	n-pentane	14.89	n-hexane	11.43
ne k	e fi	2,2-dimethylbutane	0.22	Methyl-cyclopentane	13.24
o t}	ŧ	Cyclopentane	36.9	Benzene	0.43
Ĕ	5	2,3-dimethylbutane	1.49	Cyclohexane	1.28

2036

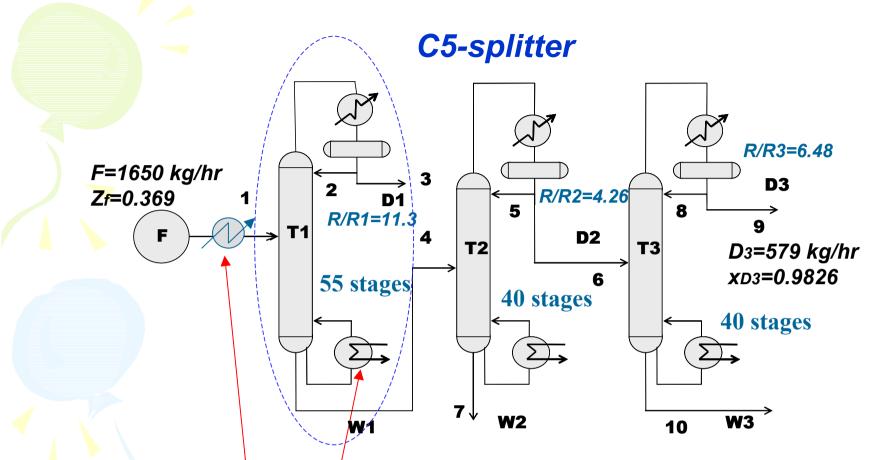
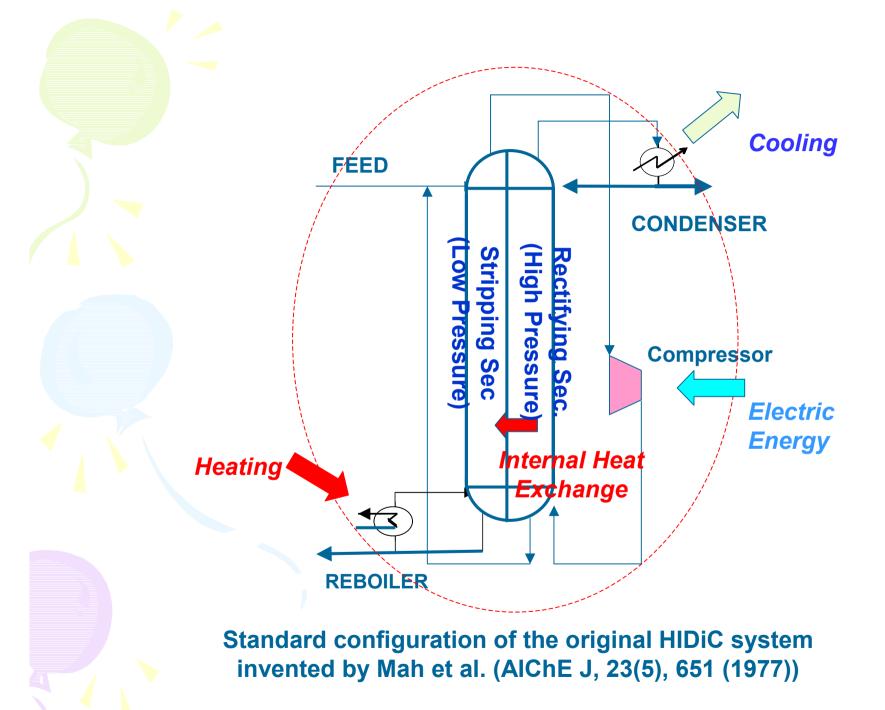


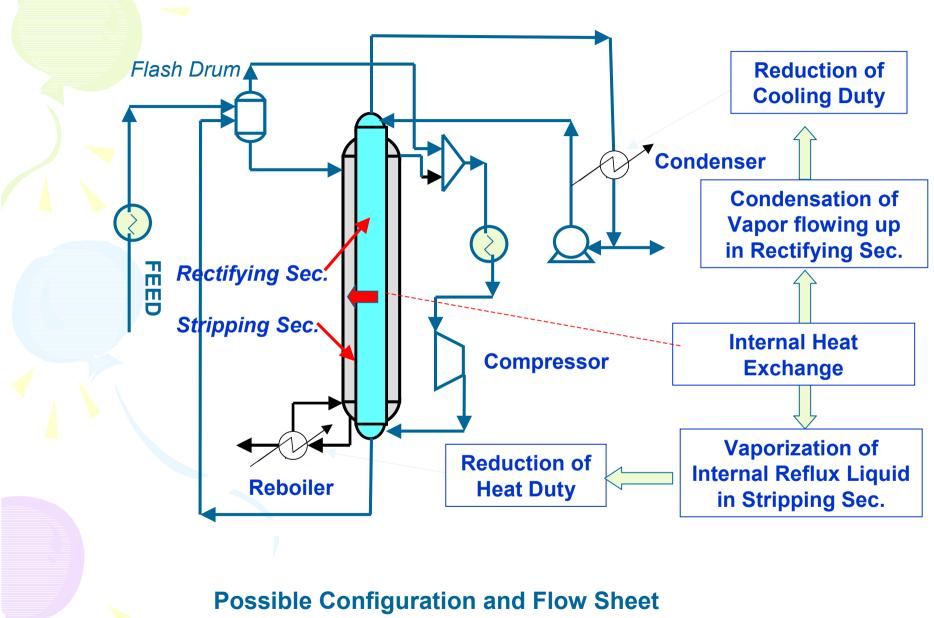
Table 2 Heat duties required for the three columns of the existing C5 splitter(Simulation results computed using the mass balance of the operation data)

	Column #1	Column #2	Column #3	Total Heat Duty
OH Condenser	-0.358 <mark>8 Gcal/hr</mark>	-0.3315 Gcal/hr	-0.3971 Gcal/hr	-1.0874 Gcal/hr
BTM Reboiler	0.3892 Gcal/hr	0.3311 Gcal/hr	0.3976 Gcal/hr	1.1179 Gcal/hr
Preheater	0.0039 Gcal/hr			

 $1 \ Gcal/hr = 10^9 \ cal/hr = 4.184 \ GJ/h$

How to reduce

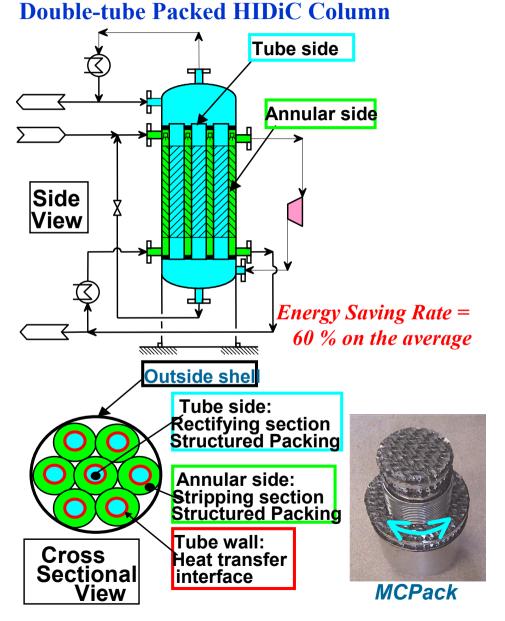




of Original HIDiC System

Commercial-scale Pilot Plant of HIDiC Serving for an Existing C-5 Splitter





2007 NEDO Project Title: Development of Compressor-free Heat Integrated Distillation System By Cascade Utilization of Vapor Pressure (Feasibility Study)

Kansai Chemical Engineering Co., Ltd Objective : Pervasion of HIDiC technology in chemical industry for prevention against global warming

(1) Possibility of great saving-rate of energy consumption
(2) Applicability to various nonideal distillation processes
(3) Possibility of trayed columns for HIDiC structure



System Design of Two or more Columns Plant

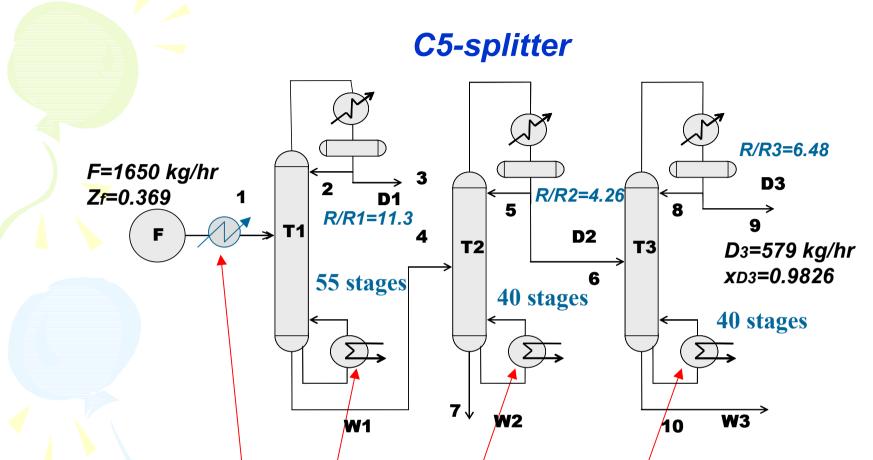


Table 2 Heat duties required for the three columns of the existing C5 splitter(Simulation results computed using the mass balance of the operation data)

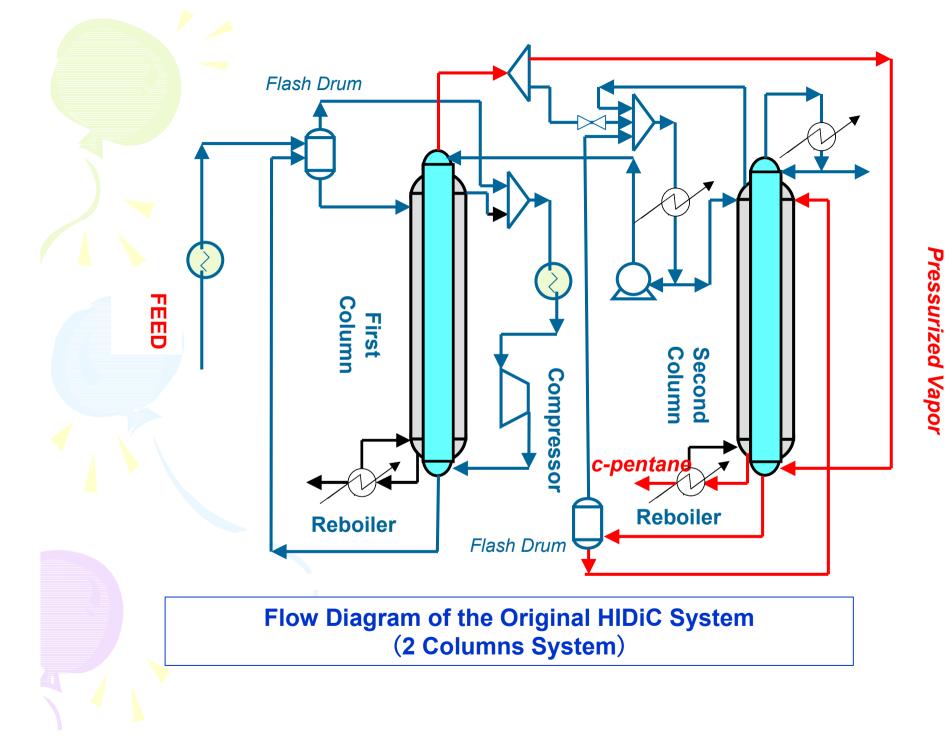
	Column #1	Column #2	Column #3	Total Heat Duty
OH Condenser	-0.358 <mark>8 Gcal/hr</mark>	-0.3315 Gcal/hr	-0.3971 Gcal/hr	-1.0874 Gcal/hr
BTM Reboiler	0.3892 Gcal/hr	0.3311 Gcal/hr	0.3976 Gcal/hr	1.1179 Gcal/hr
Preheater	0.0039 Gcal/hr			

 $1 \ Gcal/hr = 10^9 \ cal/hr = 4.184 \ GJ/h$

How to reduce

Theories and Applications of Chem. Eng., 2008, Vol. 14, No. 1

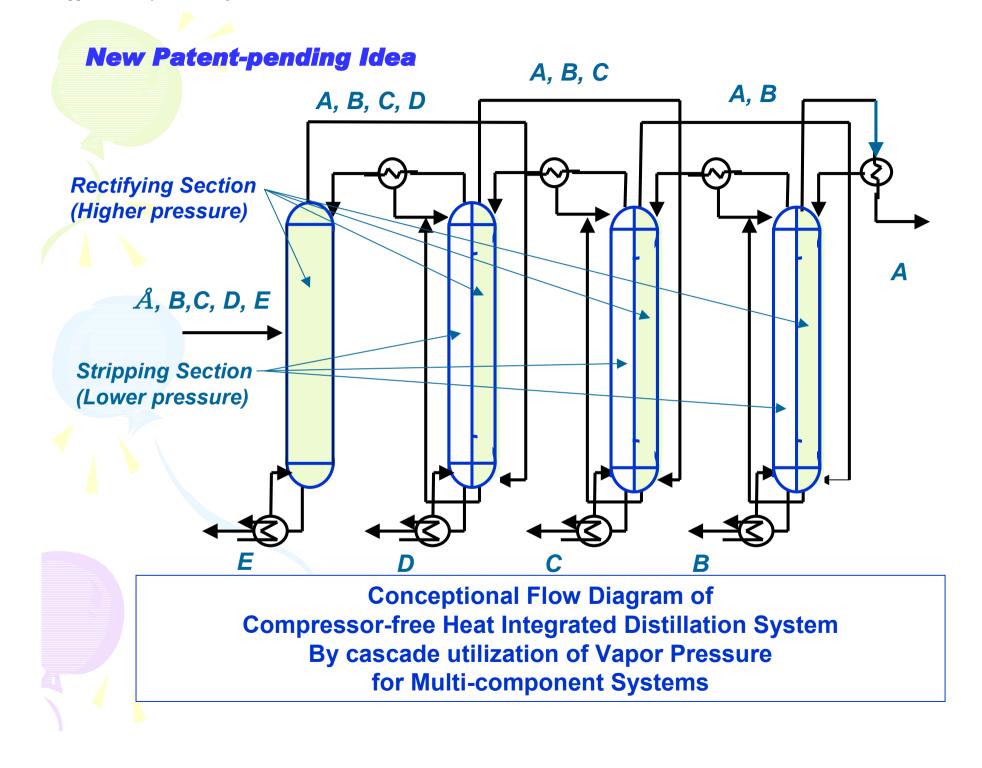


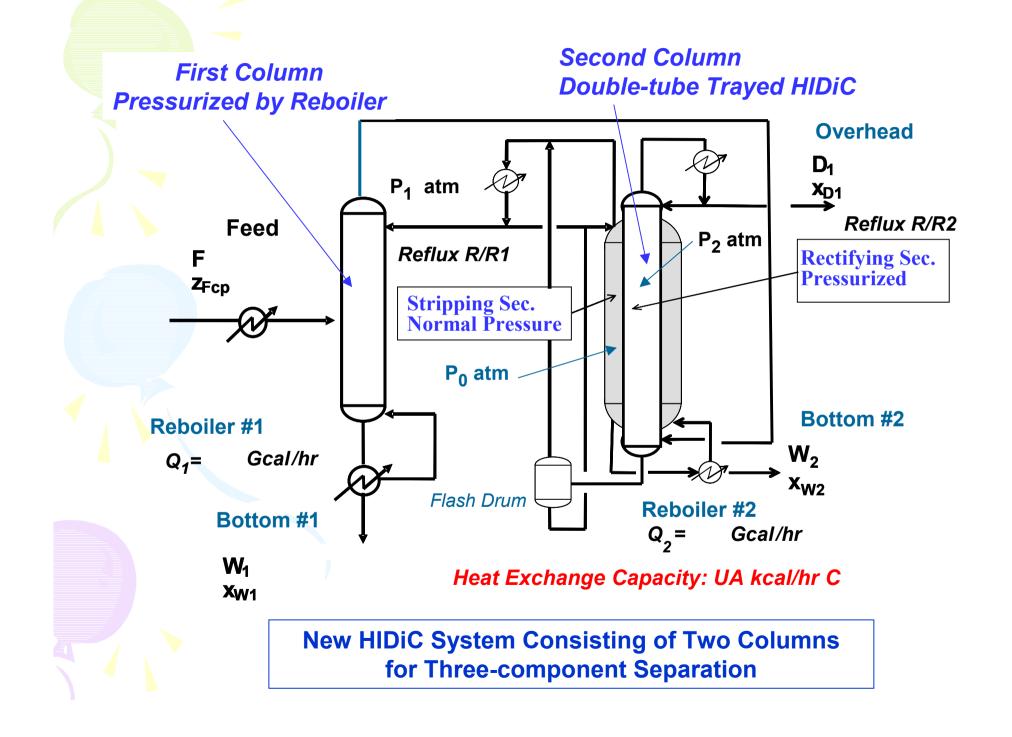


For pervasion of the heat integrated distillation technology (HIDiC Technology) in chemical industry for prevention against global warming

How to do Heat pumping without using a compressor Rectification of nonideal or dirty solution

> Invention of "Compressor-free HIDiC System"

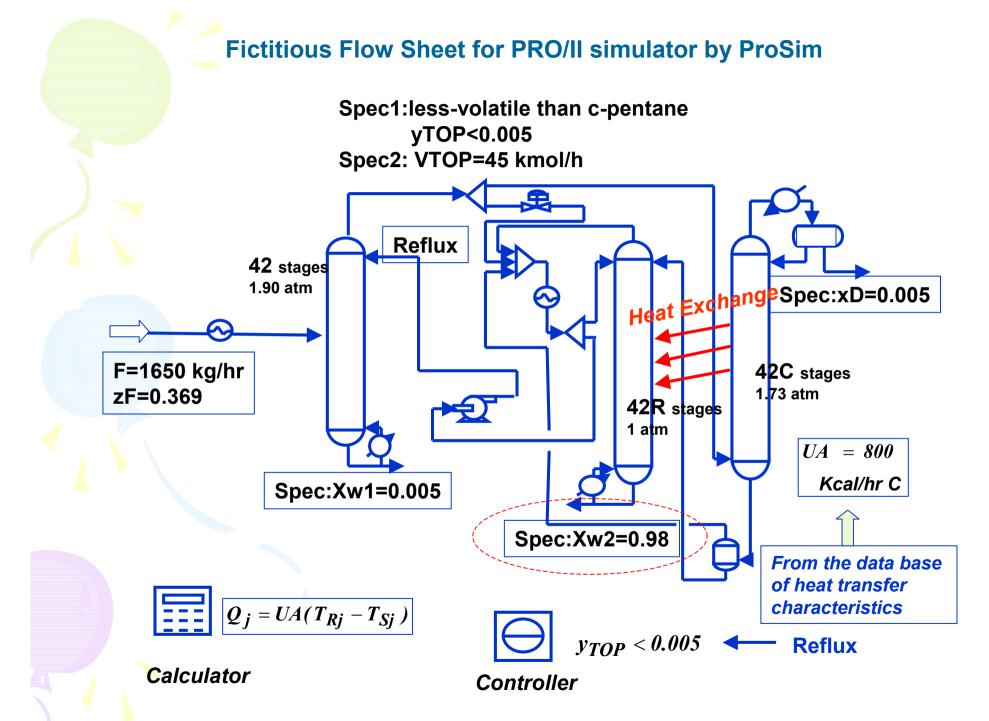




Feed Composition

Vaporized by the first column

Component	Wt%	Component W	
n-butane	0.04	2-methylpentane	13.57
i-pentane	1.80	3-methylpentane	4.71
n-pentane	14.89	n-hexane	11.43
2,2- dimethylbutane	0.22	Methyl- cyclopentane	13.24
c-pentane	36.9	Benzene	0.43
2,3- dimethylbutane	1.49	Cyclohexane	1.28



Heat Duties of the Existing C5-splitter

	Column #1	Column #2	Column #3	Total Heat Duty
OH Condenser	-0.3588 Gcal/hr	-0.3315 Gcal/hr	-0.3971 Gcal/hr	-1.0874 Gcal/hr
BTM Reboiler	0.3892 Gcal/hr	0.3311 Gcal/hr	0.3976 Gcal/hr	1.1179 Gcal/hr
Preheater	0.0039 Gcal/hr			

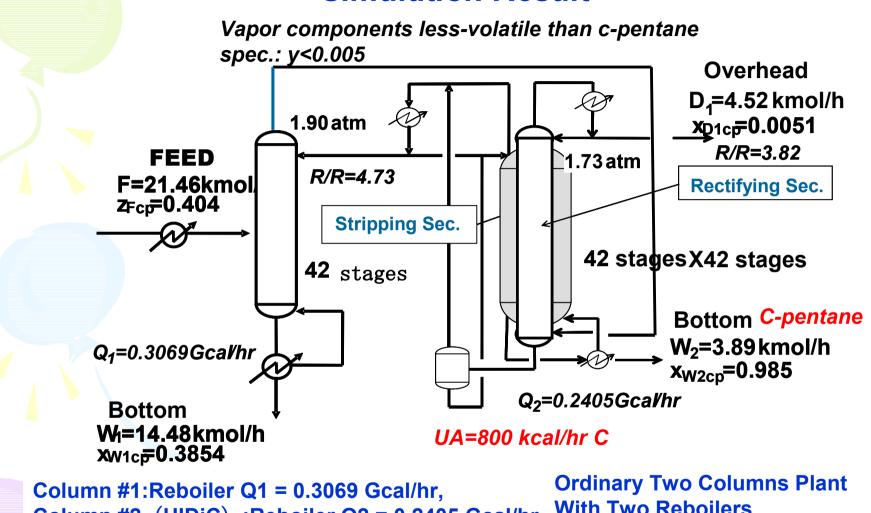
 $Es = (1 - Q_{total} / Q_{base}) \times 100 = (1 - 0.5474 / 1.1179) \times 100 = 51.03\%$

Ordinary Two Column C5-splitter and New HIDiC

	Column #1	Column #2
Two columns system of C5-splitter	0.6920 Gcal/hr	0,2317 Gcal/hr
(no internal heat integration)		
New HIDiC (Present study)	0.3069 Gcal/hr	0.2405 Gcal/hr

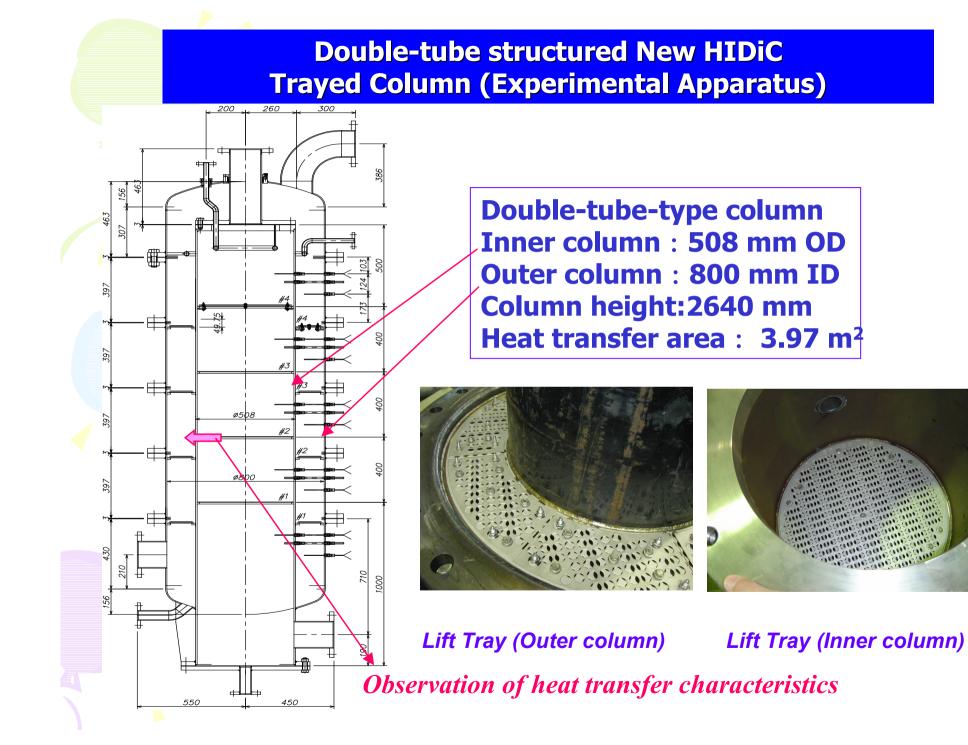
 $Es' = (1 - Q_{total} / Q_{base}') \times 100 = (1 - 0.5464 / 0.9237) \times 100 = 40.7\%$

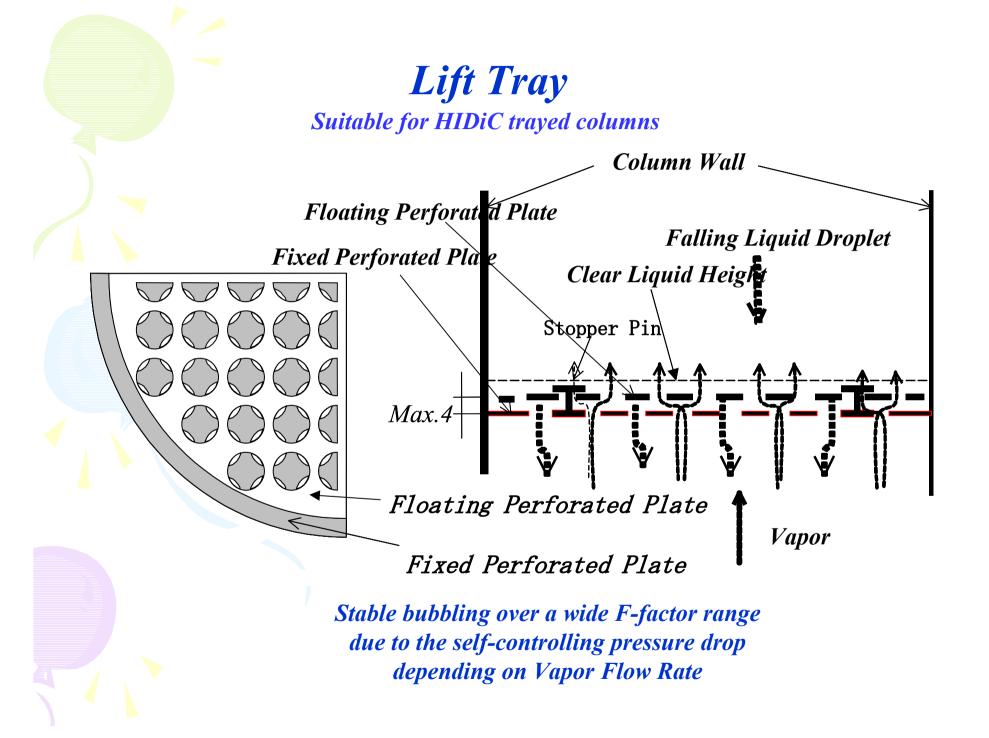
Simulation Result



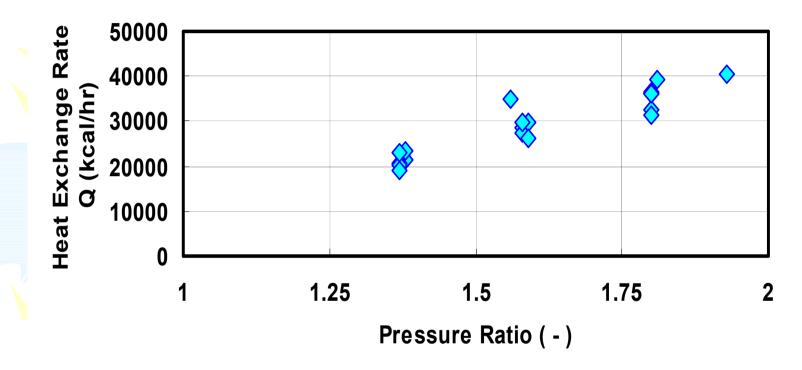
Column #1:Reboiler Q1 = 0.3069 Gcal/hr, Column #2 (HIDiC) :Reboiler Q2 = 0.2405 Gcal/hr Total Consumption : Q(total) = 0.5474 Gcal/hr Energy-saving Rate : Es = (1 - Q(total)/Q(base))x100 = 51.03 %

Ordinary Two Columns Plant With Two Reboilers Total Consumption: Q'=0.6920+0.2317=0.9237 Gcal/hr Es = (1 – Q(total)/Q')x100= 40.7 %

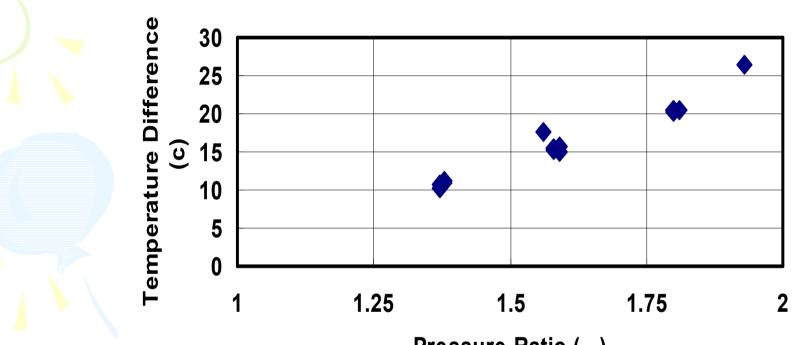




Experimental Data of Heat Transfer Characteristics For Double-tube-structured HIDiC trayed Column

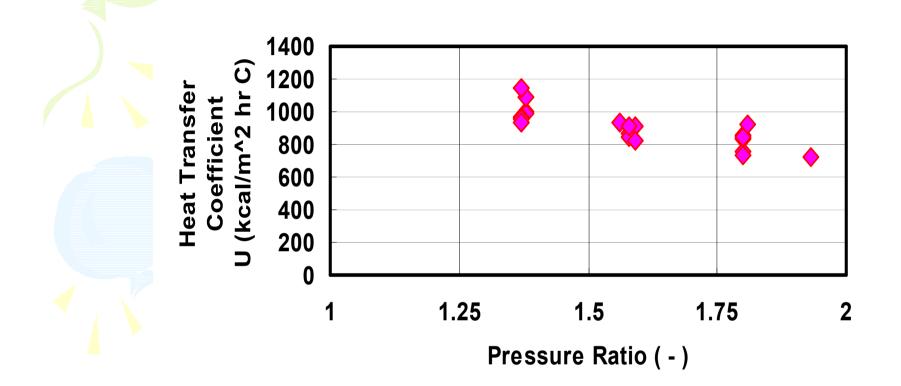


The internal heat exchange rate is proportional to the pressure ratio of the rectifying to the stripping section.



Pressure Ratio (-)

The averaged temperature difference between the rectifying and the stripping section is proportional to the pressure ratio.



The overall heat transfer coefficient has a trend slightly-decreasing With the pressure ratio increasing.

Concluding Remarks

The new compressor-free HIDiC system consisting of an ordinary column and a HIDiC-structured Column has the following advantages:

(1) The first column having no energy-saving effect has a role to supply a pressurized vapor into the next HIDiC rectifying section for heat pumping.

(2) The overhead condenser of the HIDiC stripping section has a role to reflux to the top of the first column.

(3) The next HIDiC-structured column has a great energy-saving effect.

(4) This system can widely be applied to various distillation processes such as dirty or sticky and corrosive systems as well as clean systems.



SYMPOSIUM Energy-saving Distillation Technology For Prevention Against Global Warming

Scope

This topical conference is dedicated to distillation hardware related work in the field of energysaving distillation technology. Typically, these methods cover:

- ① Heat integrated distillation column or diabatic distillation column techniques
- ② Vapour recompression techniques
- ③ Heat-coupling and dividing wall column techniques
- **④** Reactive distillation

Chairman Dr. Kunio Kataoka (Chairman) Executive Director Kansai Chemical Engineering Co., Ltd 2-9-7 Minami-nanamatsu-cho, Amagasaki 660-0053, Japan E-mail : <u>kataoka@kce.co.jp</u>

Professor Zarko Olujic (Co-chairman)

Process & Energy Department Delft University of Technology Leeghwaterstraat 44 2628 CA Delft The Netherlands E-mail: <u>z.olujic@tudelft.nl</u>