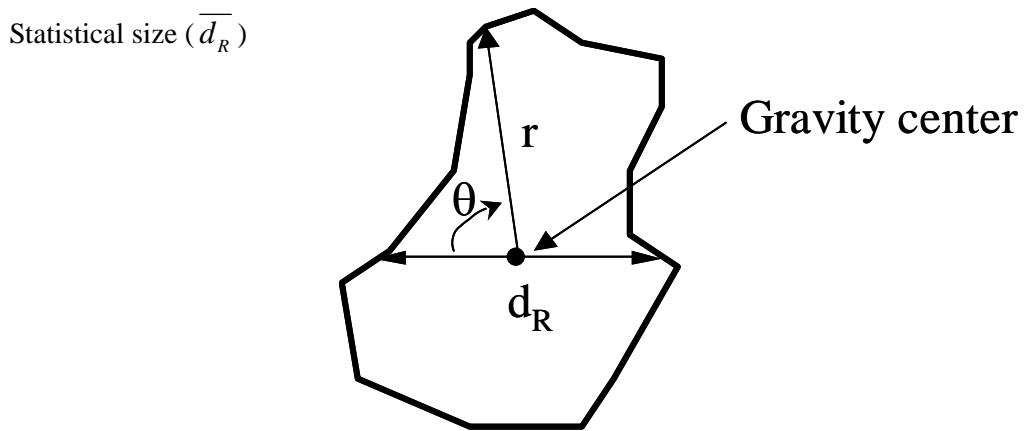


## 7. Number balance and size distribution modeling

### - Particle size



$$\overline{d_R} = \frac{1}{\pi} \int_0^{2\pi} r d\theta$$

### cf) Definition of Diameter

volume diameter, surface diameter, projected diameter, Feret diameter, Martin's diameter, Stoke's diameter, etc.

### Method of Analysis

Microscopy, sieve, settling, gas adsorption, Coulter counter, Inertial separation, light scattering etc.

### - Mean particle size

#### 1) Number-length mean diameter

$$d_{NL} = \frac{\sum N_i d_i}{\sum N_i}$$

#### 2) Geometrical mean diameter by number

$$d_{GN} = \log_{10} \frac{\sum N_i \log_{10} d_i}{\sum N_i}$$

3) Number-surface mean diameter

$$d_{NS} = \left( \frac{\sum N_i d_i^2}{\sum N_i} \right)^{1/2}$$

4) Number-volume mean diameter

$$d_{NV} = \left( \frac{\sum N_i d_i^3}{\sum N_i} \right)^{1/3}$$

5) Length-surface mean diameter

$$d_{SL} = \frac{\sum N_i d_i^2}{\sum N_i d_i}$$

6) Length-volume mean diameter

$$d_{VL} = \left( \frac{\sum N_i d_i^3}{\sum N_i d_i} \right)^{1/2}$$

7) Surface-volume mean diameter

$$d_{VS} = \frac{\sum N_i d_i^3}{\sum N_i d_i^2}$$

8) Volume-moment mean diameter

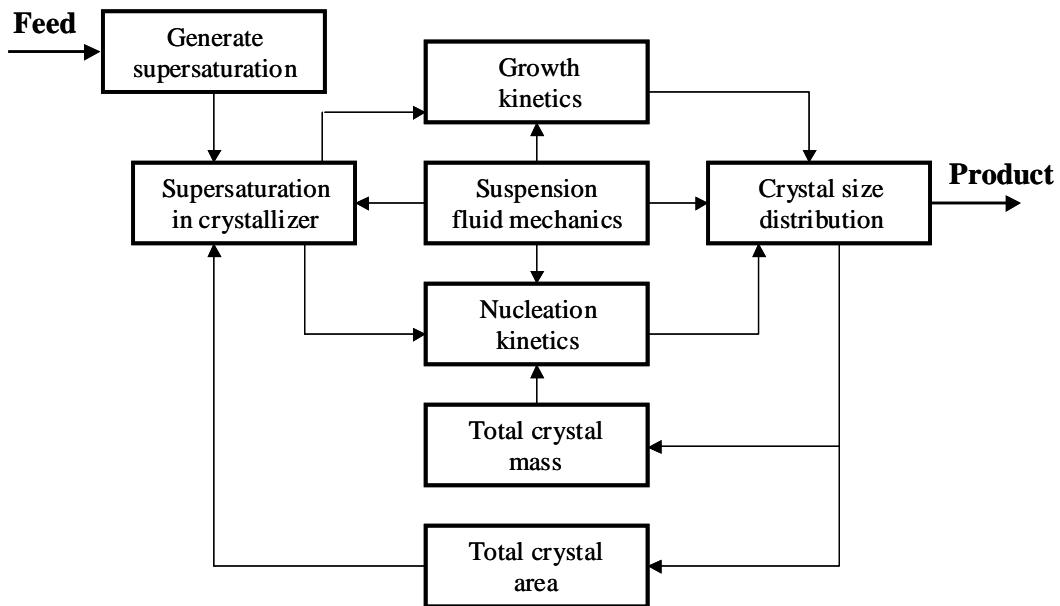
$$d_{VM} = \frac{\sum N_i d_i^4}{\sum N_i d_i^3}$$

#### **- Particle morphology**

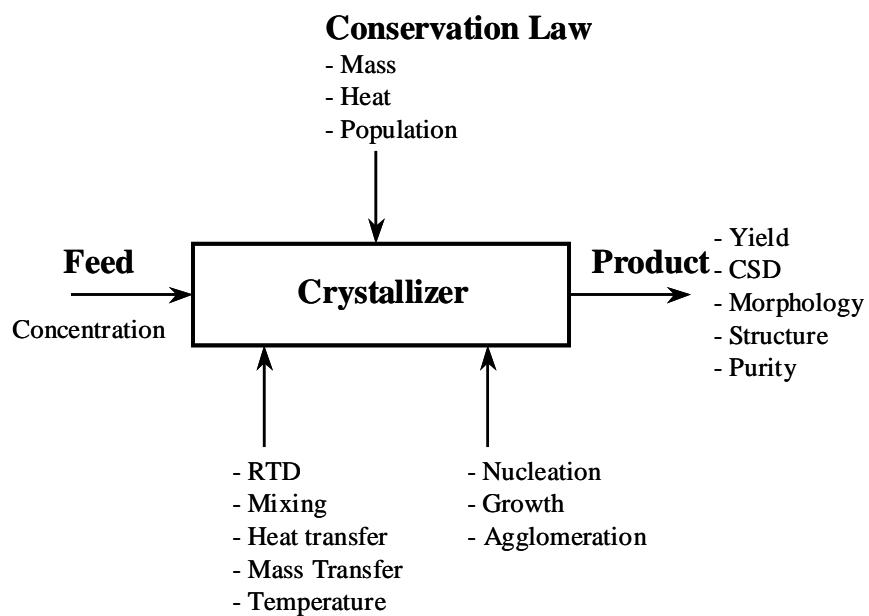
Sphere	one dimension	diameter
Cylinder	two dimension	diameter and length
Cube	one dimension	length
Irregular	many dimensions	

## 7.1 The importance of crystal size distribution

- *Inter-relationship of crystal size distribution with crystallization kinetics.*



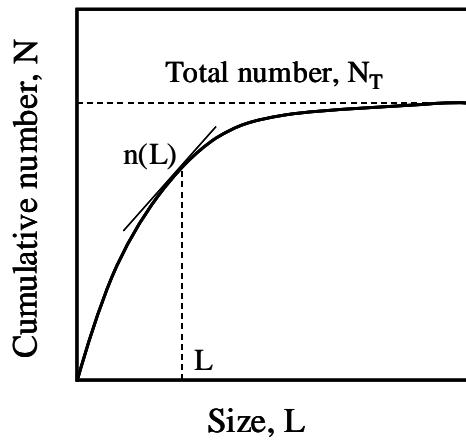
- *Conservation laws for modeling the crystallizer*



## 7.2 Characterization of size distribution

- **Number of crystals,  $N(L)$**

$N(L)$  is the number of crystals that are smaller than size  $L$  in unit volume of suspension.



- **Population density,  $n(L)$**

$$n(L) = \frac{dN(L)}{dL}$$

- number of crystals in size range  $dL$ ;  $dN = n dL$

- number of crystals in size range  $L_1$  to  $L_2$ ;  $N_{1,2} = \int_{L_1}^{L_2} n dL$

- total number of crystals in distribution;  $N_T = \int_0^{\infty} n dL$

- **Family of mean size;  $\bar{L}_{j,0}$  and  $\bar{L}_{j,j-1}$**

$$\bar{L}_{j,0} = \left[ \frac{\int_0^{\infty} L^j n dL}{\int_0^{\infty} n dL} \right]^{1/j} = \left[ \frac{\mu_j}{\mu_0} \right]^{1/j}$$

$$\bar{L}_{j,j-1} = \left[ \frac{\int_0^\infty L^j n dL}{\int_0^\infty L^{j-1} n dL} \right] = \frac{\mu_j}{\mu_{j-1}}$$

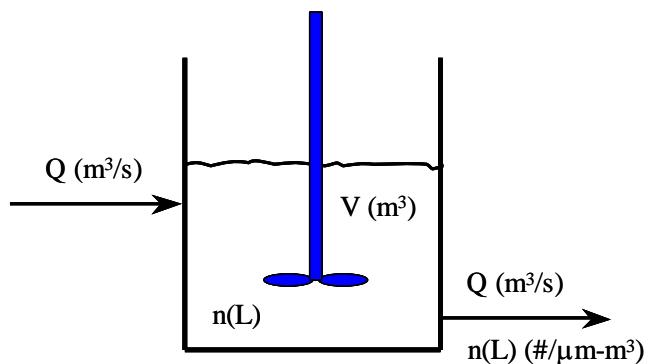
where  $j$ th moment of distribution is defined as,

$$\mu_j = \int_0^\infty L^j n dL$$

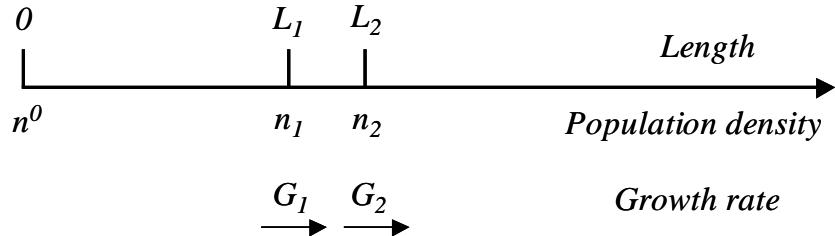
### 7.3 The continuous mixed suspension mixed product removal (MSMPR) reactor

#### *- Basic assumptions*

- 1) Continuous operation
- 2) Steady state
- 3) Perfect mixing of liquid and suspension
- 4) No classification of suspension in outlet streams
- 5) No crystals in inlet streams
- 6) No breakage and agglomeration
- 7) Same shape of crystals in whole range of size
- 8) Size-independent growth rate (McCabe's  $\Delta L$  Law)



- Population balance in control scale and volume of  $\Delta L$  ( $=L_2-L_1$ ) and  $V$



$$\text{Input rate} - \text{output rate} + \text{generation rate} = \text{Accumulation rate}$$

$$\text{Input rate of population} : n_1 V G_1 \Delta T$$

$$\text{Output rate of population} : n_2 V G_2 \Delta T + \bar{n} Q \Delta L \Delta T$$

$$\text{Generation rate of population} : 0$$

$$\text{Accumulation rate of population} : 0$$

Then,

$$n_1 V G_1 \Delta T = n_2 V G_2 \Delta T + n Q \Delta L \Delta T$$

$$\frac{n_2 G_2 - n_1 G_1}{\Delta L} = -\frac{Q}{V} \bar{n}$$

As  $\Delta L \rightarrow 0$ ,

$$\frac{dnG}{dL} = -\frac{Q}{V} n$$

By McCabe's  $\Delta L$  law,

$$\frac{1}{n} \frac{dn}{dL} = -\frac{1}{G\tau}$$

where

$$\tau = V/Q$$

Solution,

$$n = n^0 \exp\left(-\frac{L}{G\tau}\right)$$

Boundary condition

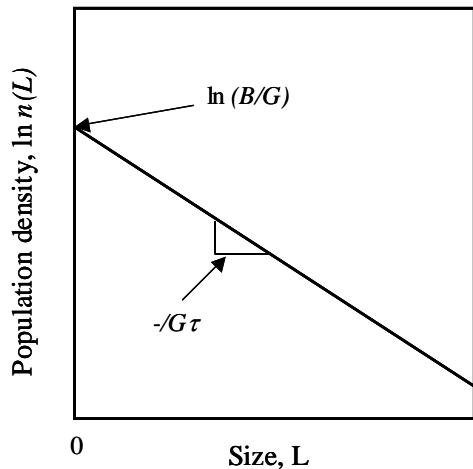
$$n(L) = n^0 \quad \text{at } L=0$$

Definition of nucleation rate (B)

$$B \equiv \frac{dN(L)}{dt} \Big|_{L=0} = \frac{dN}{dL} \Big|_{L=0} \frac{dL}{dt} \Big|_{L=0} = n^0 G$$

Therefore,

$$n = \frac{B}{G} \exp\left(-\frac{L}{G\tau}\right)$$



#### - Other distributions

Total population of crystals

$$N_T = \int_0^\infty n dL = \int_0^\infty \frac{B}{G} \exp\left(-\frac{L}{G\tau}\right) dL = B\tau$$

Total length of crystals

$$L_T = \int_0^\infty L n dL = \int_0^\infty L \frac{B}{G} \exp\left(-\frac{L}{G\tau}\right) dL = BG\tau^2$$

Total area of crystals

$$A_T = \int_0^\infty \beta L^2 n dL = \int_0^\infty \beta L^2 \frac{B}{G} \exp\left(-\frac{L}{G\tau}\right) dL = 2\beta BG^2\tau^3$$

Total mass of crystals (=magma density)

$$M_T = \rho_{cry} \int_0^\infty \alpha L^3 n dL = \int_0^\infty \alpha L^3 \frac{B}{G} \exp\left(-\frac{L}{G\tau}\right) dL = 6\alpha BG^3\tau^4$$

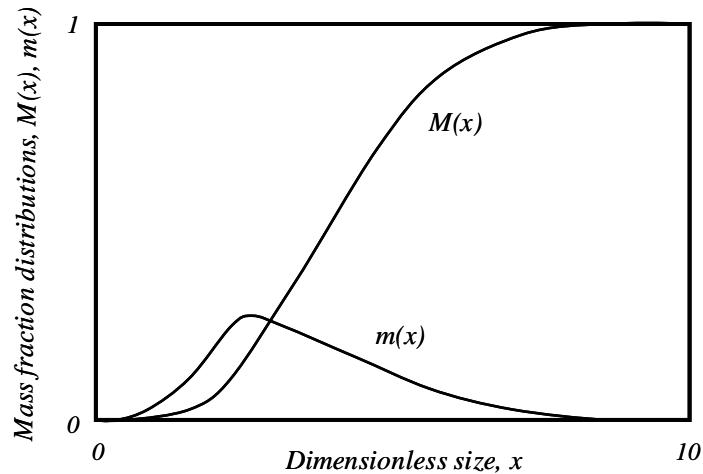
Cumulative mass fraction distribution ( $M(x)$ )

$$M(x) = \frac{M(L)}{M_T} = \frac{\int_0^x x^3 \exp(-x) dx}{\int_0^\infty x^3 \exp(-x) dx} = 1 - \left(1 + x + \frac{x^2}{2!} + \frac{x^3}{3!}\right) \exp(-x)$$

where  $x=L/G\tau$ .

Differential mass fraction distribution ( $m(x)$ )

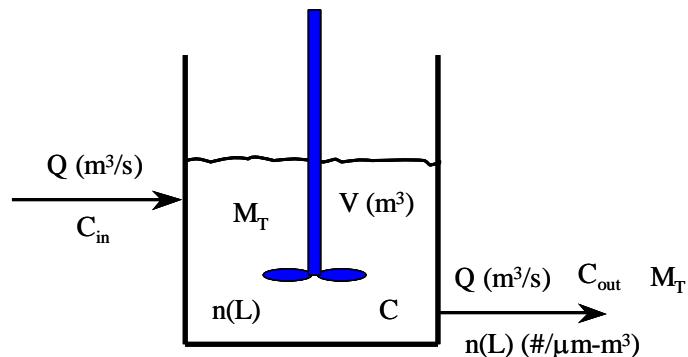
$$m(x) \equiv \frac{dM(x)}{dx} = \frac{x^3}{3!} \exp(-x)$$



The median (at  $x=0.5$ ) ;  $\overline{x_M} \equiv \frac{\overline{L_M}}{G\tau} = 3.67$

$$\overline{L}_{4,3} = \left[ \frac{\int_0^\infty L^4 n dL}{\int_0^\infty L^3 n dL} \right] = 4G\tau$$

### - The mass balance



Input rate :  $QC_{in}$

Output rate :  $QC_{out} + QM_T$

Generation rate : 0

Accumulation rate : 0

$QM_T$  is equal to amount of solute transformed to solid state.

$$QM_T = 3\rho_{cry} \frac{\alpha}{\beta} GA_T V = Q(C_{in} - C_{out})$$

Then,

$$G = K \frac{(C_{in} - C_{out})}{\tau A_T}$$

Since  $G \propto \Delta C$ ,

$$\Delta C = K_1 \frac{(C_{in} - C_{out})}{\tau A_T}$$

